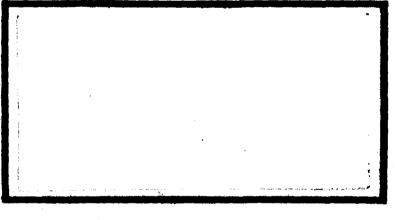
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Missile combat crew vehicles are the highest mileage accumulators within SAC and, in the interest of energy conservation, Vice CINCSAC has initiated a long-term study examining utilization of more fuel efficient crew vehicles. This thesis extends the SAC study by determining if alternate dispatch procedures and routes of travel, using currently assigned vehicles, would result in fuel conservation. A network routing model is used to determine the routes of travel for three deployment strategies and five vehicle types at the Minot AFB, ND test base. Fuel efficiency for these fifteen alternatives, measured as gallons of fuel consumed per passenger, is compared with the existing missile combat crew routing network. This study found that ten of the fifteen vehicle/deployment strategy combinations, when employed over the shortest authorized routes of travel that were developed, provided improvement over the fuel efficiency of the MCC routing system that was in effect as of 31 August 1979. The largest potential savings amounted to 52% or 26,255 gallons of fuel per year.

THE FUEL EFFICIENT MISSILE COMBAT CREW ROUTING NETWORK

A Thesis

Presented to the Faculty of the School of Systems and Logistics of the Air Force Institute of Technology

Air University

In Partial Fulfillment of the Requirements for the Degree of Master of Science in Logistics Management

By

Edward O. Jacques, Jr., BA, MBA Captain, USAF

Michael G. Woolley, BS Captain, USAF

June 1980

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has been accepted by the undersigned on behalf of the faculty of the School of Systems and Logistics in partial fulfillment of the requirements for the degree of

MASTER OF SCIENCE IN LOGISTICS MANAGEMENT

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We dedicate this work to our wives, Sudie and Patricia, and to our children, Andy and Michelle, whose patience, support, and understanding enabled us to weather this very difficult year.

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Chapter 1

INTRODUCTION TO RESEARCH

Background

Each day within the Strategic Air Command (SAC), missile combat crews (MCCs) dispatch from each of the nine strategic missile wing support bases (SMSBs) to launch control facilities (LCFs) in the surrounding area (Figure 1-1). Normal dispatch procedures have these MCCs drive government

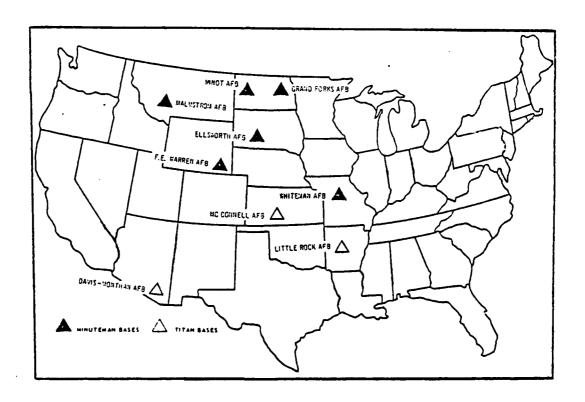


Figure 1-1 SAC Missile Bases

vehicles as their means of transportation from the strategic missile support base to and from the LCF. Because of the large number of miles driven each year by the SAC MCCs, the transport of these MCCs has arrived in the limelight of our nation's energy conservation efforts.

Problem Statement

During these days of increased emphasis on the efficient use of energy, everyone should be conscious of ways to make maximum use of the available vehicle fuel we possess because of its limited availability and rapidly rising cost. Recent presidential memorandums have addressed the necessity to reduce energy consumption within the federal government (21). These memorandums dictate the need for an overall review of government vehicle programs in an effort to find ways to increase usage utility, while at the same time reducing total energy consumption. Such a review requires special emphasis in areas of operation that accumulate high mileage. Because the transport of MCCs is the highest mileage accumulator within SAC, this area of high energy consumption requires special attention within the overall energy conservation effort (22:1).

Excessive fuel consumption associated with the transportation of missile combat crews can be caused by a combination of using vehicles with inefficient fuel consumption characteristics over transportation networks that do not minimize distances traveled. In the equipment area, the Vice Commander In Chief of SAC has recently initiated a study into more fuel efficient vehicles for deploying MCCs which also encompasses the investigation of more fuel efficient engines and alternative vehicle fuels. This study is a long-term effort specifically designed to upgrade the fuel efficiency of those vehicles used in the transporting of MCCs, but will also aid in upgrading the fuel efficiency of all vehicles in the SAC fleet. Because this study is a long-term effort whose benefits will not be realized for several years, there is the immediate short-term problem that concerns the most efficient use of the vehicles that are presently on hand. These vehicles will continue to be used until replacement is required and more fuel efficient vehicles can be procured. The purpose of this research is to look at this short-term aspect of fuel efficiency. A routing network algorithm will be used to determine if the MCC routing system that was in use as of 31 August 1979 at Minot AFB, ND is the most energy efficient means, in terms of gallons of fuel per passenger, for dispatching the MCCs to the various LCFs. It is anticipated that this method of analysis used to study the situation at Minot AFB could be applied to any missile wing's routing network through incorporation of wing-peculiar variables.

Overview

Standard station wagons were the primary mode of transporting missile combat crews to the LCFs at all missile bases until 1972. This type of vehicle had a life expectancy of 70,000 to 90,000 miles, but had poor operating characteristics (i.e., poor steering, vehicle sway, and frequent bottoming-out when fully loaded with passengers and related equipment) (24:1). The low-silhouette carryall was selected as the replacement for the station wagon and has remained the primary missile combat crew transport vehicle because of its flexibility, reliability, and long life of 170,000 to 200,000 miles. Although this vehicle has proved to be ideal for this transportation requirement, increased Environmental Protection Agency requirements have resulted in larger engines and increased antipollution components which adversely affected fuel consumption. The 1979 model year lowsilhouette carryalls are averaging only 9.5 miles per gallon as compared to prior year models which averaged over 12.0 miles per gallon (25:1).

Current MCC transport requirements vary from base to base. Each Titan base dispatches four-man MCCs to each of their 18 LCFs on a daily basis. Three to five of these MCCs are also accompanied by two-man Security Police Alert Response Teams. Each Minuteman base also dispatches a MCC to each of their 15 or 20 LCFs on a daily basis. The dispatch

may include one two-man MCC destined for one LCF; two two-man MCCs destined for two separate LCFs; or one two-man MCC, accompanied by a cook and a facility manager (FM), destined for one LCF. The literature review, personal experience, and discussion with responsible personnel did not indicate that quantitative approaches have been used as decision-aiding tools for the development of dispatch routes designed to minimize distances traveled in the transportation network. Apparently, dispatch routes have evolved through the years based on qualitative criteria such as maintaining squadron integrity and the quality of life of the MCCs.

The SAC study currently underway is concerned with the long-run fuel efficiency problem. Study members recognize that the low-silhouette carryall has proven to be an excellent vehicle with a good maintenance record, overall low cost per miles driven and high mileage life expectancy. However, the low fuel efficiency and variable crew/cargo composition of many dispatches no longer justifies the use of the low-silhouette carryall in all situations. Therefore, "the most desirable mode of transportation may have to become secondary to the most fuel efficient mode [22:2]."

SAC is approaching the study from several different perspectives. First, SAC has tasked the nine missile wings with using assigned compact station wagons and sedans for MCC transport whenever possible. These vehicles can be supplemented by low-silhouette carryalls when passenger/cargo

requirements or inclement weather conditions dictate (22:2). Second, a test program with six types of leased subcompacts at four missile bases is underway to evaluate this range of vehicles in different climatic conditions. The ultimate goal is to identify vehicles for future incorporation in a vehicle mix with low-silhouette carryalls (28:1). Third, SAC has asked HQ AFLC/LO to help in the procurement of more fuel efficient vehicles and to explore the possibility of more fuel efficient engines which could be used in the present fleet as replacement engines are required (25:1). SAC has also asked for assistance in raising the initial vehicle acquisition price ceiling based on fuel efficiency considerations within a life cycle cost framework for the procurement of these vehicles (25:2). Finally, SAC is investigating diesel powered vehicles as well as alternative fuels that might be used to supplement or replace gasoline (24:4).

SAC's study is primarily oriented towards a long-term improvement in fuel efficiency of the SAC vehicle fleet. The dividends of this study are years away. In the mean time, managers must attempt to maximize the use of our available gasoline resources. The identification of the best routing network for the transport of MCCs will pay dividends both now and in the future. By establishing the routing network with the lowest gallons of fuel per passenger ratio, our present vehicle utility is maximized and a solid foundation is established that will be enhanced by the use of more fuel efficient vehicles in the future.

Scope

In the realm of fuel efficiency there are a myriad of aspects to consider. The study initiated by the Vice Commander In Chief of SAC is an in-depth analysis concerned with improving the existing fuel efficiency of the vehicles used to transport missile combat crews to the launch control facilities. The study is investigating the potential use of more efficient vehicles in the transport process, the possibility of retrofitting existing gasoline-engine carryalls, and the use of other fuels (propane, gasahol, and natural gas) to power these vehicles. Furthermore, it is considering these aspects in conjunction with other related factors that include:

- (1) Missile Combat Crew "Quality of Life",
- (2) Severe Weather Conditions.
- (3) Vehicle Dispatch Mix,
- (4) Vehicle Ground Clearance,
- (5) Vehicle Maintenance and Acquisition Costs,
- (6) Unimproved and Paved Roads,
- (7) Crew Travel Related Time Costs,
- (8) Personnel and Cargo Volume, and
- (9) Weight Carrying Capability (7).

These aspects and related factors are beyond the scope of this research. In addition, non-routine MCC travel in response to standardization evaluations, training, or helicopter dispatches will not be addressed. The SAC study does not address the specific dispatch procedures and routes of travel to and from each LCF because these factors are under the control of each individual missile wing commander. It is within this area that we wish to extend the study of fuel efficiency by looking at the routing networks used to dispatch the MCCs to the LCFs. This study will first develop:

- (1) The shortest authorized routes from the SMSB to the LCFs.
- (2) The shortest authorized route from any LCF to any other LCF.

Using this information, this study will then consider several routing networks to determine:

- (1) The shortest authorized route from the SMSB to several LCFs with subsequent return to the SMSB.
- (2) The routing networks for available vehicles, given the constraints of the number of passengers demanded by the authorized route and the passenger/gear capacity of the vehicle.

The criterion for measurement of the various routing networks will be gallons of fuel used per passenger.

Through this criterion, the various routing networks generated will be compared, in terms of fuel efficiency, to the present MCC routing network at the Minot AFB, ND test base. It was recognized that during the course of this research, modifications might occur in the existing system due

to changes in dispatch procedures, road closings, or due to any number of other reasons. Therefore, in order to establish a single standard for comparison and to isolate out the interaction effects of future network modifications, the present MCC routing network is hereafter defined as that network and associated dispatch procedures in effect as of 31 August 1979.

Research Question

The following research question was developed to provide direction for this research: Is the present missile combat crew routing network at Minot AFB the most fuel efficient method in terms of gallons of fuel per passenger using the existing vehicles assigned to the base?

Survey of Principle Techniques

The MCC routing problem is one which falls within the scope of the well known sequencing theory problem called the Traveling Salesman Problem (TSP). The prototype TSP involves an individual who wishes to visit each of several given cities once and only once, and who also wishes to return to the starting point of his journey. The TSP has been given a great deal of study, and the literature reviewed has presented many treatises and analyses on the subject that deal with different methods to solve various TSPs. Two surveys of TSP literature were extremely helpful in directing

the researchers to studies that might be applicable to the MCC routing problem. A general synopsis of the studies presented in these surveys is presented here; however, more indepth reviews of particular methods or procedures are contained in Chapter 2 in order to maintain continuity with the subject matter being presented.

R. H. Mole, in his article that surveys routing methodology (30), indicated that Pierce (31) and Christofides (6) describe some strategies that can be used in TSP partial enumeration schemes to ensure vehicle and route feasibility.

Mole further stated that Eilon and Christofides (13) utilized a 3-optimality improvement routine on several initial feasible sets of routes and selected the best one. Dantzig and Ramser (10) developed procedures which rely on successive aggregation of a large number of very elementary routes to minimize the miles traveled at each stage. Later these procedures were developed into a "savings" algorithm. Mole also pointed out that Yellow (37) used a simple segmentation into quadrants before the sequential generation of routes.

Bellmore and Nemhauser also performed a survey of TSP literature (2). They provided a general classification of solution techniques, and also provided a description of some of the proven methods (2:538). Karg and Thompson (23) developed a method for the solution of TSPs using a "nearest neighbor" rule. In contrast, Dantzig, Fulkerson, and Johnson (9) used integer programming in the solution of

TSPs. Gomory looked further at integer programming procedures using "cutting plane" constraints (15). From Gomory's contribution, Miller, Tucker, and Zemlin (29) experimented with a "cutting plane" algorithm to solve TSPs.

Bellmore and Nemhauser also addressed dynamic programming and branch and bound algorithms. Dynamic programming solution methods were developed by Bellman (1), Gonzales (16) and Held and Karp (20), while Eastman (12), Little, Murty, Sweeny, and Karel (27), Shapiro (33), and Hatfield and Pierce (18) developed branch and bound algorithms. Subtour elimination methods were conceptualized by Eastman (12) and Shapiro (33) and Gilmore and Gomory (14). Tour-to-tour improvement algorithms were prepared by Reiter and Sherman (32) and Lin (26).

Textbooks by Budnick, Mojena, and Vollman (4; 5) and Bradley, Hax, and Magnanti (3) also gave further insight into the application of some of the above-mentioned solution techniques. In addition, other potentially useful studies that were investigated are Heidler's (19) closed circuit problem and Whiting and Hillier's (36) shortest route analysis.

Chapter 2

METHODOLOGY

Introduction

As previously stated, MCC transport requirements vary from base to base. This study will concentrate on the existing MCC routing system at Minot AFB, ND, to determine if this system is the most energy efficient means, in terms of gallons of fuel per passenger, for dispatching the MCCs to the various LCFs.

The authors are closely acquainted with the routing of MCCs to the LCFs at Minot AFB because of their combined 7 years of missile combat crew experience (spanning the time frame of November 1973 to May 1979) at that base. Their combined MCC experience, their familiarity with the present MCC routing system, and their familiarity with the overall operation of the strategic missile wing, provide them with an enhanced insight into the existing routing system.

The Present MCC Routing System

The MCC routing system in use at Minot AFB as of 31 August 1979, is within the guidelines established by the 91st Strategic Missile Wing, Deputy Commander for Operations, Operating Instruction 77-2 (38). In order to strike a balance between fuel and manhour conservation, this operating instruction specifies the primary and alternate routes of travel to be used by MCCs when traveling to the LCFs.

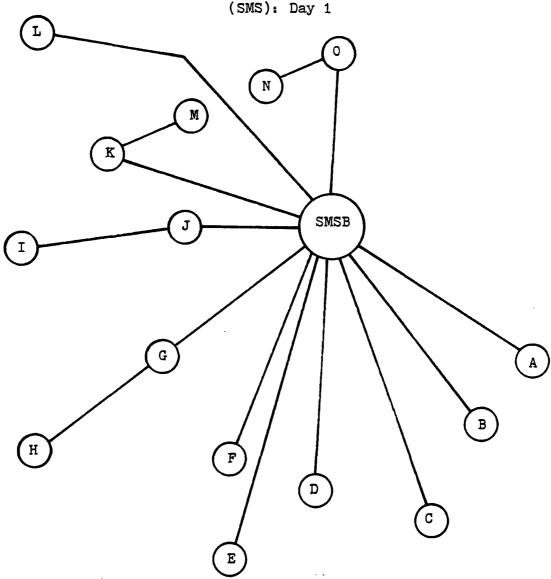
In the interest of fuel consumption, specific vehicle dispatch schedules are also identified for each of three possible dispatch requirements (38:1-2).

The second secon

These three possible vehicle dispatch schedules are based on the requirement for facility manager and cook changeover at each LCF in a specific squadron and a desire to have these personnel travel with the MCC going to the same LCF. Each day, one of the three strategic missile squadrons (740th SMS, 741st SMS, or 742nd SMS) has a scheduled changeover of facility managers and cooks. This fluctuating requirement necessitates a flexible vehicle dispatch procedure. Therefore, each of the three possible vehicle dispatch schedules are specifically identified, and the proper schedule for any particular day is contingent on which strategic missile squadron has the scheduled changeover of facility managers and cooks (38).

Figures 2-1, 2-2, and 2-3 show the three dispatch schedules of crew vehicles at Minot. Under the present vehicle dispatch scheduling system, a backtracking procedure is used. Each vehicle proceeds from the base to one or more LCFs to deliver relief personnel, and returns over the same route to pick up relieved personnel. Each vehicle presently carries one two-man MCC, two two-man MCCs, or one two-man MCC

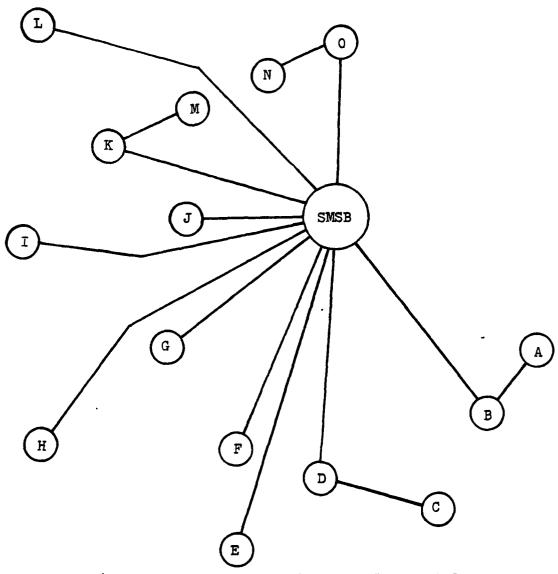
Vehicle Dispatch Schedule When Facility Manager And Cook Changeover Is In The 740th Strategic Missile Squadron



740th SMS composed of LCFs: A,B,C,D, and E. 741st SMS composed of LCFs: F,G,H,I, and J. 742nd SMS composed of LCFs: K,L,M,N, and O.

Figure 2-1 Vehicle Dispatch Schedule - Day 1

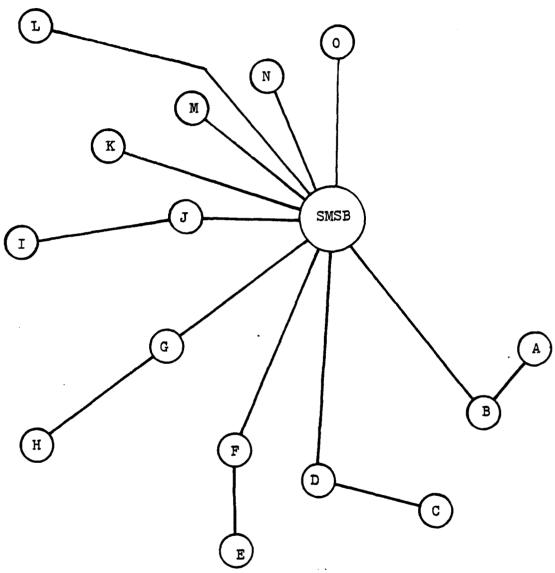
Vehicle Dispatch Schedule When Facility Manager And Cook
Changeover Is In The 741st Strategic Missile Squadron
(SMS): Day 2



740th SMS composed of LCFs: A,B,C,D, and E. 741st SMS composed of LCFs: F,G,H,I, and J. 742nd SMS composed of LCFs: K,L,M,N, and O.

Figure 2-2 Vehicle Dispatch Schedule - Day 2

Vehicle Dispatch Schedule When Facility Manager And Cook Changeover Is In The 742nd Strategic Missile Squadron (SMS): Day 3



740th SMS composed of LCFs: A,B,C,D, and E. 741st SMS composed of LCFs: F,G,H,I, and J. 742nd SMS composed of LCFs: K,L,M,N, and O.

Figure 2-3 Vehicle Dispatch Schedule - Day 3

accompanied by a facility manager and cook (38). Although the low-silhouette carryall crew vehicle can carry six personnel and their related gear, the present procedure never calls for more than four passengers in any vehicle on a regularly scheduled basis. This procedure provides flexibility for additional passenger requirements (training crew, evaluation crew, etc.) or additional equipment/house-keeping supplies. The present vehicle scheduling system satisfies driver requirements by using the MCC members in that capacity.

Because the 91st Strategic Missile Wing has three separate vehicle dispatch schedules, it was determined that the current gallons of fuel per passenger ratio could only be computed by looking at the total number of miles traveled over an entire 3-day changeover cycle. Each of the three schedules was reviewed, and distances were computed for the primary authorized routes of travel using the 91st Strategic Missile Wing (Wing III) Transport-Erector Route Book. Transport-Erector Route Book was developed by the 91st Strategic Missile Wing's Civil Engineering Squadron and Safety Office to specifically identify the available authorized routes of travel that can be used by different types of military vehicles. This document presents the entire road network that exists within the confines of the 91st Strategic Missile Wing (35). These routes were developed jointly by the Federal Highway Administration, the North Dakota

Dakota Highway Department, the United States Air Force, and local government officials during the initial development and construction of the missile wing complex (8).

The two specific types of authorized routes identified within the 91st Strategic Missile Wing (Wing III)

Transport-Erector Route Book are transport-erector routes and general access routes. Transport-erector routes are those routes that were constructed to meet the weight and safety demands required by a transport-erector vehicle (8).

This type of vehicle is used to transport a missile to various destinations within the missile wing complex. It is approximately 110 feet long, 8 feet wide, and has a gross weight of approximately 250,000 pounds when fully loaded (17). General access routes are those routes available for use by all other military traffic (35). MCCs can travel over either type of route and this study will use both types in the determination of the most efficient MCC deployment strategy.

The route book contains all authorized routes overlayed with a one square mile grid network. The distances between the SMSB and the LCFs, and the distances between the LCFs, were computed from this document. First, the distances for the existing routing system were computed (Table 2-1) by applying a mechanical divider to the routes of travel specified in the aforementioned Operating Instruction 77-2. However, these distances may or may not be the shortest

TABLE 2-1
PRESENT MCC ROUTING SYSTEM DISTANCES

Day 1 of 3-day Changeover Cycle - 740th SMS

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB - A - SMSB SMSB - B - SMSB SMSB - C - SMSB SMSB - D - SMSB SMSB - E - SMSB SMSB - F - SMSB SMSB-G-H-G-SMSB SMSB-J-I-J-SMSB SMSB-K-M-K-SMSB SMSB-K-M-K-SMSB SMSB - L - SMSB SMSB-O-N-O-SMSB	116.00 101.00 120.50 93.00 134.50 114.50 118.50 126.50 142.00 93.00 1354.00	4 4 4 4 4 2 4 4 4 0
Day 2 of 3-day Char	geover Cycle	- 741st SMS
SMSB-B-A-B-SMSB SMSB-D-C-D-SMSB SMSB - E - SMSB SMSB - F - SMSB SMSB - G - SMSB SMSB - H - SMSB SMSB - I - SMSB SMSB - J - SMSB SMSB - J - SMSB SMSB-K-M-K-SMSB SMSB - L - SMSB SMSB-O-N-O-SMSB	156.00 132.00 134.50 114.50 150.00 154.50 120.00 64.00 126.50 142.00 93.00	4 4 2 4 4 4 4 4 4 4 4 4 4 4
Day 3 of 3-day Char	geover Cycle	- 742nd SMS
SMSB-B-A-B-SMSB SMSB-D-C-D-SMSB SMSB-F-E-F-SMSB SMSB-G-H-G-SMSB SMSB-J-I-J-SMSB SMSB - K - SMSB SMSB - L - SMSB SMSB - M - SMSB SMSB - N - SMSB SMSB - N - SMSB	156.00 132.00 134.50 194.50 118.50 88.50 142.00 112.00 73.00 56.00	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4

"straight-line" methodology was applied to the TransportErector Route Book map of the 91st Strategic Missile Wing
complex to determine the shortest distance between two
points. With this "straight-line" methodology, a straight
edge was placed on the map to link any two desired points.
The shortest route between these two points was then determined by following a route of travel over authorized routes
that correspond as closely as possible with the straight
line connecting the two nodes. After determination of the
shortest routes, the distances for these routes were computed
as before using a divider and the Transport-Erector Route
book. These shortest distances will be used as data inputs
in the problem formulation.

Measure of Efficiency

The efficiency formula used within this study will be one relating the number of gallons of fuel used to transport each MCC member, facility manager, or cook to the LCF. Its basic formulation is as follows:

- (1) Compute the total number of miles (M_{total}) driven for each deployment strategy.
- (2) Divide the total number of miles driven by the fuel efficiency of the vehicle used in the deployment strategy. The fuel efficiency of each vehicle is measured by

the vehicle's miles per gallon (MPG) ratio. The result will be the total number of gallons (Gal_{total}) used within each deployment strategy/vehicle combination.

- (3) The final step is to divide the total number of gallons of fuel used for each deployment strategy/vehicle combination by the total number of passengers (Passtotal) moved within the deployment strategy.
 - (4) Symbolically, these efficiency formulas are:

(a)
$$M_{\text{total}} = \sum_{i=1}^{3} M_i$$
 Eq. 2-1

(b)
$$Gal_{total} = \frac{M_{total}}{MPG}$$
 Eq. 2-2

(c)
$$Pass_{total} = \sum_{i=1}^{3} P_i$$
 Eq. 2-3

(d) Gallons per passenger =
$$\frac{\text{Gal}_{\text{total}}}{\text{Pass}_{\text{total}}}$$
 Eq. 2-4

where, M_i = Miles driven on day i (i=1, 2, 3) for a particular deployment strategy/vehicle combination.

M_{total} = Total miles driven for each deployment strategy.

Gal_{total} = Total gallons used within a deployment strategy/vehicle combination.

P_i = Passengers transported on day i for a particular deployment strategy/vehicle combination.

Pass_{total} = Total passengers transported for each deployment strategy.

The present MCC routing system has an efficiency ratio of 3.46 gallons per passenger. It was computed using the information contained in Table 2-1 as follows:

(1)
$$M_{\text{total}} = 1354.00 + 1387.00 + 1207.00 = 3948.00$$

(3)
$$Pass_{total} = 40 + 40 + 40 = 120$$

(4) Gallons per passenger =
$$\frac{415.58 \text{ gallons}}{120 \text{ passengers}} = 3.46$$

The objective of this research is to determine if the present MCC routing system is the most efficient means, in terms of gallons per passenger, of transporting MCCs and related personnel to the LCFs. This analysis will look at several alternative deployment strategies and at several alternative vehicles for use within these deployment strategies. Our objective is to find the shortest routes of travel for the various deployment strategies and vehicles used within the strategies. From these routes, we will compute the gallons per passenger ratio to determine if there is a more fuel efficient system for routing the MCCs than the routing system presently used.

This study will focus on the types of vehicles that are presently available at Minot AFB (Table 2-2).

TABLE 2-2
PRESENTLY AVAILABLE VEHICLES

Vehicle Type (7)	MPG Rating (7)	Estimated * Passenger Capacity
Low-silhouette Carryall	9.5	6
Compact Station Wagon	18.0	4
15 Passenger Commuter Van	7.0	12 **
29 Passenger Bus	6.0	22 **
45 Passenger Bus	3.5	36 **

- *This includes MCCs, FMs, and cooks only. Motor pool drivers needed for Decision Strategy III are considered to be integral to the vehicle in use and do not impact on the estimated passenger capacity of any vehicle.
- **Passenger capacity modification would be required to enable the vehicle to also carry the personal gear associated with each crew member, facility manager, and cook (technical order bag, survival gear, and/or personal items), survival kits, and periodic housekeeping supplies carried by the facility managers. The rear seat would be removed in the vans, while the last row and one of the two seats in the second-to-last row would be removed in the two types of buses.

Although there may not presently be sufficient numbers of each type of vehicle on hand for use in the MCC routing process, it is assumed that because these vehicles have previously met the test of congressional price ceilings, that additional vehicles of these types could be procured as replacements are required.

Deployment Strategies

This study will look at three basic deployment strategies. The first deployment strategy (DS I) employs an "arrive and return" procedure called backtracking. With this strategy a vehicle proceeds from the SMSB to a location, or to a series of locations, and returns over the same path. The present MCC routing system at Minot AFB follows the premise of this deployment strategy. Figures 2-1, 2-2, and 2-3 show the backtracking routes for each day of the 3-day changeover cycle. In some situations, a vehicle departs the SMSB to one LCF and returns over the same route with the relieved personnel. In other situations, a vehicle departs the SMSB with two destinations. The vehicle proceeds to the first LCF and drops off the MCC. livery process entails approximately five minutes. vehicle then proceeds to its second destination. After the crew changeover has been completed at the second LCF, which takes approximately one hour, the relieved MCC backtracks the route to pick up the relieved crew at the first

destination and the two MCCs return to the SMSB. The apparent advantages to this strategy are that crewmembers can accomplish the driving to and from the LCF without the need of a separate driver and that a complete wing changeover can be accomplished each day. The apparent disadvantage is that the number of vehicles required to accomplish the wing changeover is greater than with other deployment strategies under investigation.

The second deployment strategy (DS II) does not employ the concept of backtracking, but rather an "arrive and wait" procedure. With this strategy, a vehicle departs the SMSB to an LCF. Upon arrival, the vehicle "waits" for the newly delivered MCC to replace the on-duty MCC. changeover process takes approximately one hour. The relieved MCC then accompanies the vehicle to the next LCF. This "arrive and wait" process is repeated until all desired locations have been visited, and then the vehicle returns to This process does not allow for the return to any previously visited LCFs. Its apparent advantages are that crewmembers can accomplish the driving to and from the LCF and that the total number of miles is reduced. However, its apparent disadvantage is that the process results in one hour waits at each LCF visited that are in addition to the required travel time. This reduces the number of LCFs that could be visited each day and might adversely affect crew availability for future alert scheduling requirements.

The third deployment strategy (DS III) that will be investigated is one that uses a trailing vehicle. A vehicle driven by a motor pool driver dispatches from the SMSB carrying MCCs destined for several LCFs. The vehicle proceeds to each LCF and drops off a MCC. As previously mentioned, this delivery process takes approximately five minutes. The vehicle continues to the next location and delivers the MCC. The process continues until all MCCs are deployed. At this point the vehicle returns to the SMSB without any relieved MCCs. One hour (the approximate length of a MCC changeover) after the first vehicle departed to deliver the new MCCs, a second vehicle is dispatched over the same route to pick up the relieved MCCs and return them to The apparent advantages of this procedure are that the MCCs are promptly and efficiently picked up for return to the SMSB and more LCFs could be visited each day with fewer vehicles. The apparent disadvantages of this procedure are that motor pool drivers would be required to drive the vehicles and the total number of miles driven would increase.

The important thing to recognize in evaluating the advantages and disadvantages of these deployment strategies is that they must be viewed in context with the whole model. Although total miles may increase with the selection of a strategy, they may be more than offset by use of a vehicle with a much higher miles per gallon ratio. This study will

evaluate these strategies in terms of the entire effect of the strategy and the associated vehicles on the gallons per passenger ratio.

Problem Formulation

The minimum distance TSP can be formulated as a 0-1 integer programming problem. The decision variable X_{ij} is an indicator variable that represents whether or not the link from node i to node j is included in the minimum tour (the shortest route through the network). X_{ij} equals one (1) if the tour includes the link from node i to node j, and X_{ij} equals zero (0) when the link from node i to node j is not included in the minimum tour. C_{ij} is the distance or "cost" associated with including the link from node i to node j in the tour. The objective is to minimize the tour distance or "cost", and becomes in general form:

Minimize
$$Z = \sum_{i,j}^{n} \sum_{i,j}^{n} C_{i,j} X_{i,j}$$
 Eq. 2-5

where n equals the number of nodes (including the starting point) in the network.

There are three sets of constraints typically associated with the Traveling Salesman Problem (4:286). The first set of constraints is introduced to assure each city is visited exactly one time. The general formula for these constraints is:

n

$$\Sigma$$
 $X_{ij} = 1$ for $j = 1, 2, ..., n$. Eq. 2-6
 $i=1$
 $i \neq j$

The second set of constraints assures there is exactly one departure from each of the n nodes. The general formula for these constraints is:

$$\sum_{\substack{j=1\\j\neq i}}^{n} X_{ij} = 1$$
 for $i = 1, 2, ..., n$. Eq. 2-7

The third set of constraints is used in order to prevent subtours (a tour which does not visit each node in the system at least once). These constraints state that if the link from node i to node j is included in the tour, then the link from j to i is excluded. For example, to prevent a subtour between nodes 1 and 2, the constraint:

$$X_{12} + X_{21} \le 1$$
 Eq. 2-8

would be used.

In problems where the number of nodes (n) is even, the number of constraints needed to prevent subtours increases at an increasing rate corresponding to the formula (5:131):

$$\frac{n!}{(n-2)!2} + \frac{n!}{(n-3)!3} + \cdots + \frac{n}{(n-\frac{n}{2})!\frac{n}{2}}$$
 Eq. 2-9

Equation 2-9 indicates that for an n of 16 (15 LCFs and the SMSB), 74,179,552 of the third type of constraints would be required. In problems where the number of nodes is odd, the number of subtour constraints required is even greater.

There are two integer programming programs in the Honeywell library that were available to the researchers. INTØ1 can handle only 11 constraints and INTLP can handle only 16 constraints (34). Because of these limitations on problem size, neither of these programs could handle the 74,179,552 subtour constraints required in the MCC routing problem. The search was then directed towards finding another type of algorithm which could be employed to solve the MCC routing system problem. A "branch and bound algorithm", developed by Little, Murty, Sweeney, and Karel to solve TSPs, was found that showed promise (26). It is a tour-building algorithm that calculates the minimum distance (lower bound) through a matrix reduction procedure. Because of the similarity of the Traveling Salesman Problem and DS II, this TSP algorithm will be applied to the DS II phase of our MCC analysis.

Two problems exist within DS II. The first is the passenger/gear capacity of presently available vehicles at Minot AFB. The maximum passenger/gear capacity is maintained by a bus that can transport thirty-six passengers and their associated gear. Because the daily changeover requirement at Minot AFB is 40 personnel, the largest vehicle is

not adequate to deploy all relief personnel in one trip. The second problem is one of time. Because it takes approximately one hour for MCC changeover, DS II will entail 15 hours of "waiting time" in addition to the time required for driving the total circuit. A rough estimate of the mileage from the base through all the LCFs and back to the base is 425 miles. If travel could be accomplished at a constant 55 miles per hour (which is not possible because some travel would be required on gravel roads where a 25 miles per hour speed limit is in force), it would take approximately 23 hours to complete the circuit. In addition to the excessive delay for relieved MCCs, current directives only allow a driver 8 hours of driving per 24-hour period (11).

To alleviate the problems of vehicle capacity and excessive time to complete the circuit, the network will be partitioned into smaller segments based on the number of LCFs a vehicle can transit in a day and their geographical locations. According to Bellmore and Nemhauser's survey of TSP literature (2), no algorithms have been developed that obtain optimality through use of a partitioning procedure. However, Held and Karp give some rules for selecting good partitions, and develop two partitioning procedures called local partitioning and global partitioning that can be used to obtain approximate minimum distance solutions (20).

Held and Karp's partitioning procedures were developed to permit the rapid direct solution of problems of

smaller proportion. Algorithms are combined through a method of successive approximation to provide a systematic procedure for handling large-scale problems (20:202). This procedure results in a sequence of permutations where each permutation is obtained from its predecessor by the solution of a derived subproblem of moderate size with the same structure as the given problem (20:202).

Given a permutation $P = (1 i_2 ... i_n)$ representing a route through n cities, the cities may be partitioned into U ordered sets, each consisting of cities which occur successively in P, and maintaining the same order as in P. A U-city TSP is solved in which each ordered set is treated as a city, and the cost of going from the set $(i_j i_{j+1} \dots i_{k-1} i_k)$ to $(i_1 i_{1+1} \cdots i_{m-1} i_m)$ is $A_{i_k i_1}$. The solution implies a reordering P' of P, with P' having cost less than or equal to that of P. Two types of partitioning proved to be especially useful. In local partitioning, all of the ordered sets but one consist of a single element. Therefore, the tours associated with P and P' differ only locally if they differ at all. At the other extreme, a global partition takes the U sets as nearly equal in size as possible, so that, if changes are made, they tend to be of a global nature [20:230].

Another approach to partitioning has been formulated by Karg and Thompson. Their tour building heuristic centers on a proposition that the optimal distance tour approximates a convex set in two-dimensional Euclidean space (23: 230). The reader is directed to the original source document for additional treatment of this partitioning procedure.

The partitioning procedure this study will use is a tour-building heuristic that centers on the geographical distribution of the SMSB and the LCFs. The authors

determined the personnel requirements and the number of LCFs that can be visited by each vehicle under consideration and, with their familiarity of the geographical placement of the LCFs within the missile wing complex, derived the partitions necessary for each vehicle. A more detailed description of the partitioning process is contained in Chapter 3. This geographical partitioning procedure is similar to Held and Karp's global partitioning procedure. Held and Karp used partitioning because of the large number of nodes in the particular TSP they were investigating (20:202), while this study used partitioning because of vehicle passenger/gear capacity and travel time constraints.

It is noted that the TSP algorithm will also be applied to the DS III phase of our MCC analysis. That is, the optimal route as determined by the TSP algorithm for the lead vehicle will also be used for the trailer vehicle.

Algorithm Application

The computer program (Appendix A) that this study will use in the analysis of the MCC routing network is the Closed Circuit Problem written by Captain Claire D. Heidler, USAF, as modified by Woolley/Jacques to permit repetitive iterations (19). Captain Heidler's Closed Circuit Problem is the computerization of an algorithm commonly known as the Little Branch and Bound Algorithm (19). This algorithm was developed to aid in the solution of traveling salesman

problems. A general summary of the algorithm follows; however, the interested reader is referred to Little (27) for an in-depth analysis of the algorithm.

The traveling salesman or closed circuit problem involves an individual who wishes to visit each of several given cities once and only once and to return to the starting point of his journey (26:2245). This procedure is descriptive of DS II and DS III. The objective is to determine the proper visiting order of the cities that will minimize the total distance he must travel. To determine the optimum route, the distances (or other measurements such as cost or time) between all cities or nodes must be known (26:2245).

An explanation of the algorithm that will be used in this study will be centered around the narrative explanation of a practical example. This example includes specific distances so that the reader may more easily follow the computational flow within the algorithm. To lend reality to the example situation, a portion of the Minot AFB complex will be used. The following computational procedures are paraphrased from Heidler's Closed Circuit Problem (19) using the example data.

Step 1: Establish a distance matrix (Figure 2-4). In this example the distances between Minot AFB, and Alpha (A), Bravo (B), and Charlie (C) LCFs will be used.

	SMSB	A	В	С	
SMSB	M	58.00	50.50	60.25	
A	58.00	M	27.50	46.50	
В	50.50	27.50	M	19.00	
C	60.25	46.50	19.00	M	

Figure 2-4. Initial Matrix

An M (representing infinity) is placed on the main diagonal as a penalty to insure that a "traveler" entering a node must depart that node.

Step 2: Reduce the initial matrix by determining the shortest distance in each row and subtracting that shortest distance from every other element in the row being investigated. This reduction operation creates at least one "zero" entry in each row. Now determine the shortest distance in each column, including the zeros resulting from the row reduction. Subtract the smallest distance in each column from every distance in the column being investigated. The result of the matrix reduction is shown in Figure 2-5.

	SMSB	A	В	C	Amount Subtrac From Its Row	
SMSB	M	0	0	9.75	50.50	
A	0	M	0	19.00	27.50	
В	1	1	M	0	19.00	
c	10.75	20.00	0	M	19.00	
Amount Subtract From Its Colum		7.5	0	0		38.00
TIOM ICS COTOM	11				116.00	154.00

Figure 2-5. Matrix After Reduction

Additionally, the distances that are subtracted from their rows and their columns should be annotated on the matrix (Figure 2-5) and summed to provide a "lower bound" or minimum distance for all tours. The "lower bound" sum can also be annotated on a pictorial representation of the iteration process called a branching diagram (Figure 2-9).

Step 3: Identify the zero (0) cells in the reduced matrix presented in Figure 2-5. For each zero (0) cell located, identify the smallest distance, other than the zero itself, in the cell's associated row and column. In Figure 2-5, a zero (0) is found on the bottom row for the (C,B) cell. The smallest distances are 10.75 for the row and 0 for the column. These two distances represent minimum penalties for not choosing the zero cell. These two distances should be summed and annotated in the zero cell associated with the calculation. Therefore, the penalty for cell (C,B) is 10.75 + 0 = 10.75. Figure 2-6 shows the matrix with the penalties for each zero cell.

	SMSB	A	В	<u> </u>
SMSB	М	0 1	0 0	9.75
A	0 1	M	0 0	19.00
В	1	1	M	0 10.75
C	10.75	20.00	0 10.75	M

Figure 2-6. Matrix With Penalties

Step 4: In order to minimize overall circuit distance, the objective is to avoid incurring large penalties. The penalties represent the extra mileage incurred if that particular route is not taken. Therefore, the first tour link is determined by selecting the zero cell with the highest penalty. Because the matrix is symmetrical around the main diagonal, the routes with the highest penalty of 10.75 are actually both the same and reflect a tour link of B to C or C to B. In the case of ties, the algorithm allows one to arbitrarily choose among the ties. Therefore, in our example, the route from B to C is chosen. After selection of the highest penalty, add the penalty to the "lower bound" on the branching diagram and delete the associated row and column for that tour link from the matrix. This procedure is seen in Figures 2-7 and 2-9.

	SMSB	A	В	
SMSB	M	0	0	
A	0	M	0	
C	10.75	20.00	0	

Figure 2-7. Matrix With Column and Row Deleted

Step 5: Now assign an infinite distance to the reverse of the tour link generated in Step 4. Because we selected a tour link from B to C in the example, the tour link from C to B, cell (C,B), would be assigned an infinite

distance (M) to preclude choosing the same link. Figure 2-8 shows the results of this manipulation.

	SMSB	A	В	
SMSB	M	0	0	
A	0	M	0	
C	10.75	20.00	M	

Figure 2-8. Matrix After Step 5

Step 6: This completes the first iteration of the algorithm. To continue the process and generate the next tour link, return to Step 2 with the Step 5 matrix and reiterate the process until only one link remains in the matrix.

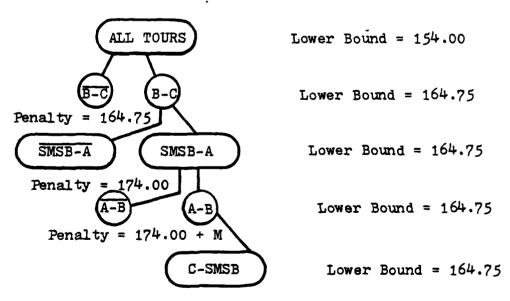


Figure 2-9. Branching Diagram
The shortest tour is SMSB-A-B-C-SMSB.

A brief summary of the cverall route determination sequence is provided for the reader.

Step 1: Establish the distance matrix.

Step 2: Reduce the matrix - rows first, then columns. Then sum the distances subtracted in the reduction process.

Annotate this sum on the branching diagram.

Step 3: Calculate penalties for each zero (0) cell.

Step 4: Select the cell possessing the highest penalty as the next tour link, and delete its row and column from the matrix. Add the penalty to the lower bound and annotate the branching diagram.

Step 5: Assign an infinite distance to the reverse of the link generated to establish a new matrix.

Step 6: Repeat Steps 2 through 5 until only one link remains.

Figure 2-9 shows the results of the continuation of the example. The process has indicated that the shortest route that will encompass all four points and return to the starting point is based on a tour from SMSB-A-B-C-SMSB that encompasses 164.75 miles. However, this is only one solution. There is a remote possibility that the left branch generated on the first iteration can branch to a better solution. This is only true if the lower bound for the first left branch is less than the final lower bound calculated by continually branching to the right. An interesting

phenomenon is that "if the TSP is symmetric and t is any tour, another tour with the same cost is obtained by traversing the circuit in the reverse direction [26:484]."

Therefore, if the initial matrix at Step 1 is symmetrical, then not only is the tour produced by the algorithm optimal, but the reverse tour is also optimal. In the example the tour was SMSB-A-B-C-SMSB. Thus, since the initial matrix is symmetrical, the tour SMSB-C-B-A-SMSB is also optimal. For a more detailed description of the computer program's logic, the interested reader can reference the original source document (19).

When the geographical partitioning procedure is used, the segmentation of the network will be accomplished prior to the input of the distance matrix into the computer program. The input of the distance matrix applicable only to a particular segment will ensure an optimal solution for that partition.

As stated earlier, Little's Branch and Bound Algorithm and Heidler's Closed Circuit Problem aid in the solution of problems within DS II and DS III. Heidler's model solves the general Traveling Salesman Problem where a vehicle proceeds from a starting point and visits each node only once and subsequently returns to the starting point. However, Heidler's computer model does not solve the "arrive and return" procedure (backtracking) inherent to DS I. With the backtracking procedure of DS I, a vehicle proceeds from

a starting point and visits each node. The vehicle stops at the last node in the network and returns to the starting point via the reverse route. Figure 2-10 and Figure 2-11 give pictorial representations of these concepts.

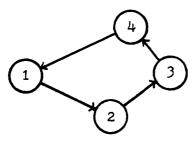


Figure 2-10. Traveling Salesman

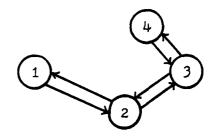


Figure 2-11. Backtracking

The authors have developed the following heuristic to handle the multiple visits required by the backtracking procedure. It is based on the symmetrical property of Little's Branch and Bound Algorithm.

Step 1: Solve the routing problem using the Heidler computer program. It will yield two equivalent solutions because of the symmetric property.

Step 2: Select the solution that has the longest last link (the link from the last LCF back to the SMSB).

Step 3: Subtract the last link from that solution. This provides the shortest tour that visits all nodes without returning to the starting point.

Step 4: Multiply the result by two. This will incorporate the "backtrack" and will provide the least total distance for that routing problem.

Using the previous example from Figure 2-4, we found the optimal tour was SMSB-A-B-C-SMSB (solution 1) or SMSB-C-B-A-SMSB (solution 2). The total distance for both solutions was 164.75 miles. The link C-SMSB (solution 1) is 60.25 miles while the link A-SMSB (solution 2) is 58.00 miles. Subtracting the longer link of C-SMSB (solution 1) from 164.75 gives 104.50 miles.

Summary

The objective of this research is to determine if the present MCC routing system is the most efficient means, in terms of gallons per passenger, of transporting MCCs and related personnel to the LCFs. Three alternate deployment strategies will be examined for each of the five vehicle types presently available at Minot AFB. Deployment strategy I involves an "arrive and return" procedure called backtracking, where a vehicle visits each LCF in the tour discharging relief personnel and backtracks over the same route picking up relieved personnel. Deployment strategy II incorporates an "arrive and wait" procedure where the vehicle waits at each LCF for crew change and returns to the SMSB from the last LCF visited. Deployment strategy III is similar to DS II; however, a trailing vehicle is used to pick up relieved personnel. An appropriate algorithm will be used to develop the shortest route network for each deployment strategy. Heidler's computer code of the Little Branch and

Bound algorithm will be used to determine the shortest route network for DS II and DS III. This program, together with the heuristic developed to handle multiple LCF visits, will be used to determine the shortest route network for DS I. Geographic partitioning will be used to determine which LCF will be included in the network being analyzed under each deployment strategy/vehicle type combination.

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Once the shortest routes are determined for each vehicle type/deployment strategy, the gallons per passenger measure of efficiency will be computed to determine if there is a more fuel efficient system for routing the MCCs than the routing system presently used. Table 2-3 summarizes the 15 vehicle type/deployment strategy combinations that will be investigated where the response variable gal/pax; is the gallon per passenger measure of efficiency of vehicle type i (i = 1,...,5) and deployment strategy j (j = I,...,III).

TABLE 2-3

GALLONS PER PASSENGER MEASURES OF EFFICIENCY

VEHICLE TYPES

DEPLOYMENT STRATEGIES

	DS I	DS II	DS III
Low-Silhouette Carryall	Gal/Pax ₁ I	Gal/Pax ₁ II	Gal/Pax ₁ III
Compact Station Wagon	Gal/Pax _{2I}	Gal/Pax _{2II}	Gal/Pax _{2III}
Commuter Van	Gal/Pax _{3I}	Gal/Pax _{3II}	Gal/Pax _{3III}
29 Passenger Bus	Gal/Pax _{4I}	Gal/Pax _{4II}	Gal/Pax _{4III}
40 Passenger Bus	Gal/Pax _{5I}	Gal/Pax _{5II}	Gal/Pax _{5III}

Chapter 3

DATA COMPUTATION AND ANALYSIS

Data Computation

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The straight-line methodology was applied to the Transport-Erector Route Book map of the 91st Missile Wing complex (Figure B-1 in Appendix B provides a facsimile map of the 91st Strategic Missile Wing complex) to determine the shortest distance between two specific points over authorized The routes of travel between the SMSB and the LCFs were determined, as well as the routes of travel between all combinations of LCFs. From these shortest authorized routes of travel, the distances between the SMSB and the LCFs, as well as between all combinations of LCFs, were computed. These shortest authorized routes of travel and corresponding distances are detailed in Tables C-1 through C-16 in Appendix C and the routes of travel distances for the entire wing complex are summarized in Table D-1 in Appendix D. Due to the scale of the Transport-Erector Route Book map and the accuracy of the mechanical divider, the authors recognize a potential measurement error of approximately one-half $(\frac{1}{2})$ mile per every 100 miles. However, since this constitutes a measurement error of only \emptyset .5%, study results are not significantly affected.

Because of vehicle capacity constraints and the travel time constraints to complete the circuit, the wing complex was partitioned into smaller segments. A geographical partitioning procedure was used which considered the geographical location of the LCFs, the personnel requirements for the LCFs on each day of the 3-day changeover cycle, and the personnel capacity restrictions of the vehicle under study. The authors evaluated these factors and developed partitions that would maximize vehicle capacity (to reduce the total number of vehicles required) as much as possible.

THE PROPERTY OF STREET

After development of the required partitions, the appropriate algorithm was used to develop the shortest authorized route network for each deployment strategy. For DS II, the appropriate distances associated with the shortest authorized routes between the SMSB and the LCFs and between the LCFs were input into Heidler's computer program of the Little Branch and Bound algorithm to determine the shortest authorized route networks and the route distances. Because of the "trailing vehicle" concept of DS III, the shortest authorized route networks for DS III were the same as those for DS II, but the route distances were twice that of DS II. The heuristic developed in Chapter 2 to handle multiple LCF visits was used to determine the shortest authorized route network for DS I. The partitions, route network sequences, route network distances, and the numbers of people

transported in each vehicle for each vehicle/deployment strategy combination are contained in Tables E-1 through E-15 in Appendix E.

The total distances, number of gallons of fuel used, and the gallons per passenger efficiency formulation for each vehicle/deployment strategy combination for each 3-day chargeover cycle are summarized in Tables 3-1, 3-2, and 3-3. The results of the investigation indicate that 10 of the 15 vehicle/deployment strategy combinations provide greater fuel efficiency than the 3.46 gal/pax of the present MCC routing system.

TABLE 3-1
VEHICLE/DEPLOYMENT STRATEGY SUMMARY - TOTAL MILES

Type of Vehicle	DS I	DS II	DS III
Carryall	3,265.00	2,961.00	5,922.00
Station Nagon	3,635.50	3,511.75	7,023.25
Van .	2,500.50	1,894.75	3,789.50
29 Pax Bus	2,266.00	1,424.50	2,849.00
45 Pax Bus	2,166.00	1,353.00	2,706.00

TABLE 3-2

VEHICLE/DEPLOYMENT STRATEGY SUMMARY-GALLONS OF FUEL CONSUMED

Type of Vehicle	DS I	DS II	DS III
Carryall	343.68	311.68	623.37
Station Wagon	201.97	195.10	390.18
Van	357.21	270.68	541.36
29 Pax Bus	377.67	237.42	474.83
45 Pax Bus	618.86	386.57	773.14

TABLE 3-3

VEHICLE/DEPLOYMENT STRATEGY SUMMARY-GALLONS PER PASSENGER

Type of Vehicle	<u>DS I</u>	DS_II	DS III
Carryall	2.86	2.60	5.19
Station Wagon	1.68	1.63	3.25
Van	2.98	2.26	4.51
29 Pax Bus	3.15	1.98	3.96
45 Pax Bus	5.16	3.22	6.44

Analysis of Data

Table 3-4 provides a comparison of the potential savings of the fifteen vehicle/deployment strategy combinations over the MCC routing system in effect as of 31 August 1979. The table includes the number of gallons of fuel saved (lost) and the percent savings (percent loss) by conversion to the particular vehicle/deployment strategy combination. The number of gallons of fuel saved (lost) and

the percent savings (percent loss) were derived as follows:

Proposed system

1 - efficiency ratio | Percent saved | Percent saved | Percent lost |
efficiency ratio | Percent lost | Percent lost |
efficiency ratio | Percent lost | Percent lost |
efficiency ratio | Percent lost | Percent lost |
efficiency ratio | Percent lost |
efficiency

TABLE 3-4

POTENTIAL SAVINGS PER 3-DAY CHANGEOVER CYCLE-GALLONS OF FUEL/PERCENT SAVINGS

Vehicle Type	<u>DS I</u>	<u>DS II</u>	<u>DS III</u>
Carryall	71.9/17%	103.00/25%	(207.79)/(50%)
Station Wagon	213.61/51%	220.48/53%	25.40 / 6%
Van	58.37/14%	144.90/35%	(125.78)/(30%)
29 Pax Bus	37.91/ 9%	178.16/43%	-(59.25)/(14%)
45 Pax Bus	(203.28)/(49%)	29.01/7%	(357.56)/(86%)

Our analysis indicates that five vehicle/deployment strategy combinations are less efficient than the present MCC routing system and are excluded from further consideration. These combinations include Carryall/DS III, Van/DS III, 29 Pax Bus/DS III, 45 Pax Bus/DS I, and 45 Pax Bus/DS III.

Closer analysis of the remaining ten vehicle/deployment strategies indicates that although a vehicle/deployment strategy is more efficient in terms of gallons per passenger, the choice of that combination may necessitate additional resource requirements that are beyond the existing capabilities of the base resources and may result in incremental costs which prove prohibitive.

The Station Wagon/DS III combination has a fuel efficiency ratio of 3.25 gallons per passenger. While this combination provides improvement over the present MCC routing system's 3.46 gallons per passenger, twenty vehicles would be required as well as twenty drivers to ferry the vehicles to the LCFs and back. These vehicle and manpower resource requirements may result in prohibitive incremental costs.

Inspection of the 29 Pax Bus/DS II combination indicates that the longest network that the bus would be required to follow encompasses 307.50 miles. At an average of 35 miles-per-hour, an approximation to account for travel over pavement and gravel roads, the network would require 8.79 hours of continuous travel. Because of the "arrive and wait" nature of DS II, the 8.79 hours of travel time would be augmented by one-hour waits at each of the 10 LCFs visited in the network. The total "travel" time of the longest network thus becomes 18.79 hours, and the first MCC relieved or the last MCC to be delivered could possibly spend approximately 17 hours on the bus. This long transit time, combined with the required "crew rest" period, could reduce the number of wing crews available for duty on the next duty and negatively impact crew scheduling requirements. Also, because MCC members would be required to drive the bus after a

24-hour alert tour, driving safety might be impacted. Although the 1.98 gallons per passenger is a 43% improvement over the present MCC routing system's 3.46 gallons per passenger, the potential disadvantages associated with this vehicle/deployment strategy combination must be thoroughly evaluated by wing personnel to determine if these disadvantages outweigh the advantages.

The 45 Pax Bus/DS II combination has the same disadvantages as the 29 Pax Bus/DS II combination. Its largest network of 260 miles and visits to 8 LCFs would result in a "total" travel time of 15.43 hours. While its 3.22 gallons per passenger efficiency ratio is a 7% improvement over the present MCC routing system, its potential disadvantages must also be thoroughly evaluated by wing personnel in comparison with the potential advantages.

The Van/DS II combination experiences the same types of problems. The longest network for the Van/DS II combination entails 213.00 miles and visits to 5 LCFs. At an average of 35 miles-per-hour, the "total" travel time would be 11.09 hours. While the 2.26 gallons per passenger efficiency ratio represents a 35% improvement, the potential disadvantages associated with the length of time required to tour the longest network and the necessity for a relieved MCC member to drive the van must be evaluated by wing personnel in conjunction with the potential advantages.

The Van/DS I and 29 Pax Bus/DS I combinations reflect the same disadvantages inherent with DS II combinations.

The Van/DS I combination's longest network is 291.50 miles with 9 stops required during the backtracking associated with visits to 5 LCFs. At an average of 35 miles-per-hour, with 5 minute stops at each of the 9 stopping points, the total travel time would be 9.08 hours. The 29 Pax Bus/DS I combination's longest network encompasses 527.00 miles and 19 stops at 10 LCFs. Its "total" travel time for the longest network would require 16.66 hours. The 14% and 9% improvements associated with these combinations must be evaluated by wing personnel against their lengthy travel times.

Although wing personnel must evaluate the disadvantages associated with the Station Wagon/DS III, 29 Pax Bus/DS II, 45 Pax Bus/DS II, Van/DS II, Van/DS I, and 29 Pax Bus/DS I combinations, the authors believe that the potential lengthy travel times, driving safety factor, vehicle and manpower resource requirements, and prohibitive incremental costs associated with these six vehicle/deployment strategy combinations are more disadvantageous than advantageous.

Therefore, the authors propose that the Station Wagon/DS III, 29 Pax Bus/DS II, 45 Pax Bus/DS II, Van/DS II, Van/DS I, and 29 Pax Bus/DS I combinations should not be considered unless constrained gasoline or vehicle resources force the use of one of these combinations.

The authors believe that the four remaining vehicle/deployment strategy combinations are all acceptable and preferable alternatives to the present MCC routing system.

The Carryall/DS I combination is similar to the present MCC dispatching system. The 17% improvement to 2.86 gallons per passenger is the result of increased passenger capacity from four to six, and the development of the shortest authorized routes of travel that replace the present emphasis on the use of paved roads. The Carryall/DS II combination provides a 25% savings by using shorter routes of travel and the "arrive and wait" procedure. The additional time associated with DS II adds only two hours to the "total" travel time of any network (resulting from the additional wait at two LCFs). The Station Wagon/DS I combination provides potential fuel savings of 51% as the result of its 18 miles-per-gallon rating and the shorter authorized routes of travel. Even though the total number of miles per 3-day changeover cycle for this combination is the largest of the four acceptable combinations, the increased fuel economy of the station wagon provides the second-best fuel efficiency ratio of 1.68 gallons per passenger. The Station Wagon/DS II combination provides the best overall results and provides a potential 53% fuel savings over the present MCC routing system. "arrive and wait" nature of this combination would only result in the addition of one hour to the "total" travel time of the tour provided in the Station Wagon/DS I combination.

Chapter 4

CONCLUSIONS AND RECOMMENDATIONS

Conclusions

The authors believe that the Station Wagon/DS II vehicle/deployment strategy (coupled with travel over the shortest authorized routes of travel), and its potential 52% fuel savings, would be the best choice to replace the present MCC routing system at Minot AFB, North Dakota.

The following analysis demonstrates the potential benefits of this recommendation when considered over a one year time horizon. The present MCC routing system uses 415.58 gallons of fuel for each 3-day changeover cycle, as compared to 195.10 gallons with the Station Wagon/DS II combination. The net potential savings are 220.48 gallons for each 3-day changeover cycle. With 121.67 3-day changeover cycles per year, the potential fuel savings amount to 26,826 gallons of fuel per year. With the present escalation in the price of fuel, the impact of the quantity of fuel saved is magnified by its potential savings in fuel costs. The potential yearly fuel savings for the four acceptable vehicle/deployment strategy combinations were similarly computed and are summarized in Table 4-1.

TABLE 4-1
POTENTIAL YEARLY SAVINGS OF FUEL IN GALLONS

Vehicle Type	DS I	DS II
Carryall	8,748	12,642
Station Wagon	25 , 990	26,826

It must be remembered that these potential results were a composite of the effects of the vehicle/deployment strategies, the miles-per-gallon rating of the vehicle, and the development of the shortest authorized routes of travel. These potential savings must be tempered by a recognition that these potential savings are based on day-to-day use of the shortest authorized routes of travel and the transporting of only the required LCF personnel. Severe weather, gravel and paved road conditions, and additional LCF personnel (training crews, standardization crews, visitors, etc.) may all have negative impacts on the potential savings of any of the four acceptable vehicle/deployment strategy combinations. Thus, the flexibility to meet these contingencies may prevent the actual attainment of the estimated potential savings for any vehicle/deployment strategy combination that would be used in conjunction with the shortest authorized routes of travel. However, following the shortest authorized routes of travel as often as possible will reduce overall fuel consumption.

Recommendations for Implementation

The next step in the comparison of the present MCC routing system with the four acceptable alternatives should be to independently implement the four alternatives on a trial basis to see if practical application of the procedures described in this study perform in the same manner as the study predicts. Because Minot AFB's forty-seven carryalls (7) are enough to effect wing-wide implementation of the Carryall/DS I or Carryall/DS II combinations, practical tests of these MCC routing systems over the shortest authorized routes could be done throughout the entire wing or just with a segment (such as a squadron) of the wing. Because Minot AFB's eight station wagons (7) do not meet the needs of eleven vehicles for the Station Wagon/DS I or Station Wagon/ DS II combinations, the practical tests of these MCC routing systems over the shortest authorized routes could be done through rotating segments that will aggregate to a test of the entire wing. If the results correspond to the research results, all available compact station wagons could be dedicated to the routing of MCCs, with the less efficient carryalls picking up the vacated transportation responsibilities. and additional compact station wagons could be purchased as existing vehicle assets required replacement.

Recommendations for Further Study

Although the SAC study is investigating many related factors such as alternative fuels, alternative vehicle types, and MCC "quality of life" factors, several areas appear to be logical extensions of this research. An increase in the number of passengers carried in a vehicle might reduce the total number of miles and the number of vehicles required. This might be achieved through the use of cargo roof racks or other vehicle modifications. An example of the potential of this area of study can be seen by modifying the compact station wagon to carry 6 personnel. The compact station wagon could then follow the same routes as the Carryall and the fuel efficiency ratios for DS I, DS II, and DS III would drop to 1.51 gal/pax, 1.37 gal/pax, and 2.74 gal/pax respectively. These lower fuel efficiency ratios would enhance the fuel savings to 28,471 gallons, 30,561 gallons and 10,559 gallons for DS I, DS II, and DS III.

Another area that could be investigated is the dispatching of Security Police personnel with the other LCF personnel. This would be another excellent means to cut down on overall miles traveled, fuel consumption, and vehicle requirements. Since Security Police personnel transit to the same LCFs as the MCCs, FMs, and cooks, the potential for additional wing savings might occur by coordinating the movement of all required LCF personnel in the same vehicle rather

than continuing the present system of multiple vehicle visits to the same LCF.

A third potential area for investigation is the concept of a vehicle mix. While the SAC study encompasses the concept of vehicle mix with new vehicles, a mix of the vehicles presently on hand should be analyzed to see if further economies can be achieved by using the best vehicle for each particular situation or network.

A fourth area that may be investigated is an elimination of the requirements for facility manager and cook changeover by squadrons. For example, after the present research was well underway, it came to our attention that the 91 SMW changed the present deployment strategy, which was used for comparison purposes in our research, to remove squadron in-The authors tegrity in facility manager and cook changeovers. recognize that the resultant increased utilization of the carryall with six passengers can save gasoline resources, but that use of the same routes that were in effect as of 31 August 1979 does not result in maximizing fuel savings. It is recommended that this recent change to the present MCC routing system at Minot AFB be analyzed in conjunction with use of the shortest authorized routes developed in this study to determine if further savings can be achieved.

A final area for potential investigation is to change the 24-hour alert tour to a 48 or 72-hour alert tour. A decrease in fuel consumption would directly correspond with these longer alerts. For example, an increase to a 48-hour alert tour would cut gasoline consumption for comparable MCC routing systems by one-half, while an increase to a 72-hour alert tour would cut gasoline consumption by two-thirds. Such changes in dispatch procedures would further enhance the results identified in this research. However, the reduced gasoline requirements would have to be weighed against behavioral and physical factors such as crew member morale and fatigue to determine if the benefits of such a change outweigh the costs.

As stated in the scope, this study attempted to look at the short-term problem of using the existing vehicle types at Minot AFB in the most efficient manner possible. Through the development of the shortest authorized routes of travel and fifteen vehicle/deployment strategy combinations, this study has demonstrated the potential for fuel savings of up to 53% in routing MCCs to the LCFs at Minot AFB, North Dakota. In addition, the development of the shortest authorized routes of travel should complement and enhance the findings of the SAC study by providing the shortest distances for any new or modified vehicles in the future.

The potential for savings at each missile base exists, and the methodology developed in this study appears to be capable of implementation at any of them. Any opportunity for potential fuel savings cannot be overlooked, and other SAC missile bases should consider applying this methodology in an effort to reduce their gallons per passenger fuel efficiency ratio.

APPENDIXES

The Approximation of the Control of

APPENDIX A

COMPUTER CODE FOR HEIDLER'S CLOSED CIRCUIT PROBLEM (19)

```
10
      CHARACTER FLNAME+50
      CONHON TEMP2(20), TEMP(20), T(18, 18, 30), SUN(50), K1, L1, N
20
30
      CONHON PEN(18,18,30), J1, J2, L
40
       COMMON N(50), IS
50
      CONNON KEND, LEND, NS, IN, INDX, ID1, ID, DFDR
60
      COMMON MX(40), IP
70 500 NX(1)=0
80
      IS=0
90
      DFDR=0.0; INDX=1; DFDR1=0.0; MS=0
        M=1
100
       SUM(M)=0.0
110
        PRINT 50
120
130 50 FORHAT(//,5x,"HOW HANY ROWS AND COLUMNS?")
140
      READ, K1,L1
150
       KEND=K1
160
       LEND=L1
170 100 PRINT 110
180 110 FORMAT(//, "WHAT IS THE HODE OF THE DATA INPUT (TELETYPE=1)"
            "(PERMENENT FILE=2, HALT=3)")
1904
        READ, IANS
200
210
        IFC=05
220
       IF(IANS.LT.1.OR.IANS.GT.3)GO TO 100
230
        IF(IANS.EQ.1)GO TO 130
        IF(IANS.EQ.3)GO TO 245
235
        PRINT 120
240
250 120 FORMAT(//)
260
        IFC=15
        PRINT, "INPUT DATA FILE NAME IN THE FORM
270
                                                     USERID/FILENANE;"
        PRINT, "END YOUR INPUT WITH A SEMICOLON(;)" PRINT, "EXAMPLE 75B/INPUT;"
280
290
300
        PRINT 120
310
        READ, FLNAME
320
        CALL ATTACH(15,FLNAHE,1,0,IOK,)
330
        DO 90 K=1,K1
340
        READ(IFC,1110)LN,(T(K,L,M),L=1,L1)
350 90 CONTINUE
360 1110 FORMAT(V)
370
        GO TO 25
380 130 PRINT 51
390 51 FORMAT(//,5X,"ENTER NATRIX BY ROWS AFTER=")
        READ, ((T(K,L,H),L=1,L1),K=1,K1)
400
410
     25 IF(INDX.EQ.2)CALL RESET
420
        IF(INDX.EQ.3)GO TO 45
430 14 DO 1 K=1,K1
440
        DO 2 L=1,L1
450
        IF(K.EQ.L)T(K,L,H)=1000000000.0
460
     2 CONTINUE
470
        TEMP(K)=T(K,1,H)
480
       DO 3 J=1,L1
       IF(T(K,J,N).GE.1000000.)G0 TO 3
490
```

```
500
        IF(T(K,J,H).LE.TEMP(K))TEMP(K)=T(K,J,H)
510 3 CONTINUE
520
       IF (TEMP(K),GE.1000000.)TEMP(K)=0.0
530 1 CONTINUE
540
        DQ 4 K=1,K1
550
        DG 5 L=1.L1
540
       IF(T(K.L.M).GE.1000000.)G0 TO 5
570
        IF(K.EQ.L)60 TO 5
580
       T(K,L,M)=T(K,L,M)-TEMP(K)
590 5 CONTINUE
600 4 CONTINUE
620
        DO & L=1,L1
630
        TEMP2(L)=T(1,L,N)
640
       BO 7 K=1,K1
650
       IF(T(K,L,N).GE.1000000.)G0 TD 7
660
        IF(L.EQ.K)GQ TO 7
        IF(T(K,L,N).LE.TEMP2(L))TEMP2(L)=T(K,L,N)
670
680 7 CONTINUE
       IF(TEMP2(L).GE.1000000.)TEMP2(L)=0.0
690
700
     6 CONTINUE
710
        DO 8 L=1,L1
       DO 9 K=1,K1
720
       IF(T(K,L,M).GE.1000000.)G0 T0 9
730
740
        IF(L.EQ.K)60 TO 9
750
        T(K,L,H)=T(K,L,H)-TEMP2(L)
760 9 CONTINUE
770 8 CONTINUE
790 10 FORMAT(5(F12.2.2X))
800
        DO 11 K=1,K1
810
        SUN(N)=SUH(H)+TEHP(K)
820 11 CONTINUE
830
       DO 12 L=1,L1
840
        SUM(M)=SUM(M)+TEMP2(L)
850 12 CONTINUE
840
       IF(INDX.EQ.2.AND.SUN(N).GT.DFDR)60 TO 25
870
       IF(INDX.EQ.2)GO TO 49
880
        PRINT 13, SUN(N)
890 13 FORMAT(///,15X,"THE LOWER BOUND IS ",F7.2)
900 49 CALL PENLTY
910
       IF(INDX.EQ.2)GO TO 46
        TUN (H, J2, H) H39+(H) HU2=(1+H) HU2
920
930
       PRINT 24, J1, J2
940 24 FORMAT(//,10X,"TAKE ROUTE ",12," TO ",12)
        PEN(J1,J2,H+1)=PEN(J1,J2,H)
950
960
        BO 18 K=1,K1
970
        DO 19 L=1,L1
980
       T(K,L,M+1)=T(K,L,M)
990 19 CONTINUE
1000 18 CONTINUE
1010 46 CALL XOUT
1020
        IF (KEND.LT.2.AND.LEND.LT.2)GO TO 20
```

```
1030
       KEND=KEND-1
1040
       LEND=LEND-1
1050
         GD TO 14
1060 20 IF(INDX.LT.2)GO TO 40
1070
        DFDR1=SUM(N)
1080
        DO 27 ID=1,IS,2
1090
          PRINT 13,SUN(IN+2+ID)
1100 28 FORNAT(//,10X,"TAKE ROUTE ",12," TO ",12)
1110
        PRINT 28, N(ID), N(ID+1)
1120 27 CONTINUE
1130 40 BO 21 K=1,K1
         DO 22 L=1.L1
1140
         IF(T(K,L,H).GE.1000000000.)G0 TD 22
1150
1140 23 PRINT 24,K,L
1170 22 CONTINUE
1180 21 CONTINUE
        DFDR=SUH(N)
1190
1200
        IF(INDX.GE.2)GO TO 38
1210
        ID1=IS+1
1220
        1D=1D1+1S-1
        IS=1
1230
1240
        DO 35 IL=ID1,ID
1250
        N(IL)=N(IS)
        IS=IS+1
1260
1270 35 CONTINUE
        IF (INDX.LE.1) IN=H
1280
1290 38 INDX=2
1300
         CALL RTSUM
1310
        GO TO 25
1320 45 IF(DFDR1.LE.O.O)GO TO 41
1330
        60 TO 26
1340 41 PRINT 42
1350 42 FORMAT(///,10x,"NO BETTER SOLUTION FOUND")
1360 26 PRINT 43
         FORMAT(///,10X,"THIS IS THE FINAL SOLUTION")
1370 43
         CALL DETACH(15, IOK,)
1374
1375 60 TO 500
1380 245 STOP
1390
        END
1400
        SUBROUTINE RESET
1410
        COMMON TEMP2(20), TEMP(20), T(18, 18, 30), SUH(50), K1, L1, H
        COMMON PEH(18,18,30),J1,J2,L
1420
       COHNON N(50),IS
1430
1440
        COMMON KEND, LEND, MS, IM, INDX, ID1, ID, DFDR
1450
       COMMON NX(40), IP
         M1=IH+3
1460
1470
        H=HS+2
1480
         IF(M.EQ.2)PRINT 7
1490 7 FORMAT(///.15x."BEGINNING LEFT NODE SEARCH")
1500
         IF(SUM(H).GT.DFDR)INDX=3
1510
         IF(H.EQ.H1-2)INDX=3
```

```
1520
        IF(INDX.GE.3)GO TO 3
1530
       SUM(N1)=SUM(N-1)
1540
       KEND=K1
1550
        MS=H
       LEND=L1
1560
1570
        DG 1 K=1,K1
1580
        DO 2 L=1.L1
1590
        T(K,L,M1)=T(K,L,M)
1600
      2 CONTINUE
1610
      1 CONTINUE
1620
        IS=N-2
1630
         IF(IS.GT.2)JJ=JJ+1
         IF(IS-2)5,5,6
1640
1650
     6 IT=ID1
         DO 4 KK=1, M-JJ
1660
1670
         M(KK)=M(IT)
1680
         IT=IT+1
1690
         CONTINUE
1700
      5 \text{ IF}(IS.EQ.2)JJ=3
1710
         IF(IS.EQ.2)N(1)=N(ID1)
1720
         IF(IS.EQ.2) IS=1
1730
         H=H1
1740
      MT=MS
1750
       IF(IS.EQ.0)MS=100000
1760
        CALL PENLTY
1770
       T(J1,J2,N)=1000000000.
1780
      MS=MT
1790 3
        RETURN
1800
        END
1810
        SUBROUTINE TRACX
        CONHON TEMP2(20), TEMP(20), T(18, 18, 30), SUM(50), KI, L1, M
1820
1830
        COMMON PEN(18,18,30),J1,J2,L
1840
       COMMON N(50), IS
1850
       COMMON KEND, LEND, MS, IN, INDX, ID1, ID, DFDR
1860
       COMMON NX(40), IP
1870
        TENP2(L)=1000000.
1880
        DO 2 J3=1,K1
        IF(J3.EQ.J1.ANB.L.EQ.J2)G0 TO 2
1890
        IF(T(J3,L,M).LE.TEMP2(L))TEMP2(L)=T(J3,L,M)
1900
1910 2
        CONTINUE
1920
        IF(KEND.LT.3)GO TO 3
1930
        IF(TEMP2(L).GE.1000000.)TEMP2(L)=0.0
1940 3 RETURN
1950
1960
       SUBROUTINE ROSCAN
1970
        COHMON TEMP2(20), TEMP(20), T(18,18,30), SUH(50), K1, L1, M
1980
        COHMON PEN(18,18,30), J1, J2, L
1990
       COHHON N(50), IS
2000
       COHNON KEND, LEND, NS, IH, INDX, ID1, ID, DFDR
2010
       COMMON NX(40), IP
2020
        TEMP(J1)=1000000.
```

```
2030
        DO 2 J4=1,L1
2040
        IF(T(J1,J4,N).GE.1000000.)G0 TO 2
2050
        IF(J1.EQ.J4)G0 TO 2
2040
        IF(J4.EQ.J2)G0 TO 2
2070
       IF(T(J1, J4, N) . LE. TEMP(J1)) TEMP(J1)=T(J1, J4, N)
2080 2 CONTINUE
2090
       IF(KEND.LT.3)GO TO 1
       IF (TEMP(J1).GE.1000000.) TEMP(J1)=0.0
2100
2110 1 CONTINUE
2120
        RETURN
        END
2130
        SUBROUTINE PENLTY
2140
        CORMON TEMP2(20), TEMP(20), T(18, 18, 30), SUM(50), K1, L1, M
2150
2160
        COHNON PEN(18,18,30).J1.J2.L
2170
       COMMON N(50).IS
2180
      COMMON KEND, LEND, MS, IN, INDX, ID1, ID, DFDR
2190
       COMMON NX(40).IP
2200
        DO 1 K=1,K1
2210
        DO 2 L=1.L1
2220
        PEN(K,L,M)=-1.
        IF(K.EQ.L)GO TO 2
2230
2240
       IF(T(K,L,M).GE.1000000.)G0 TO 2
2250
        IF(T(K,L,N).LE.0.0)60 TO 3
2260
        GO TO 2
2270 3 J1=K
2280
        J2=L
2290
        CALL TRACX
2300
       CALL ROSCAN
        PEN(J1,J2,M)=TEMP(J1)+TEMP2(L)
2310
2320 2
        CONTINUE
2330 1
        CONTINUE
2340
        PTEMP=PEN(1,2,N)
2350
        DO 4 K=1.K1
2360
        DO 5 L=1,L1
2370
       IF(T(K,L,N).GE.1000000.)G0 TO 5
2380
        IF(K.EQ.L)GO TO 5
2390
        IF(PEN(K,L,N).LT.0.0)60 TO 5
2400
        IF(PEN(K,L,N).GE.PTENP)GO TO &
2410
        GO TO 5
2420 & PTEMP=PEN(K,L,H)
2430
        J1=K
2440
        J2=L
2450 5 CONTINUE
2460 4 CONTINUE
2470
       IF(NS.GT.10000)G0 T0 7
2480
       IS=IS+1
       1L=(21)H
2490
       IS=IS+1
2500
2510
        N(15)=J2
2520
        PEN(J1,J2,M)=PTEMP
2530 7 RETURN
```

```
2540
       END
2550
        SUBROUTINE XOUT
2540
        CONHON TEHP2(20), TEMP(20), T(18, 18, 30), SUM(50), K1, L1, M
2570
        COMMON PEN(18,18,30), J1, J2, L
2580
       COMMON N(50), IS
2590
      CONMON KEND, LEND, MS, IN, INDX, ID1, ID, DFDR
2600
       COMMON NX(40).IP
2610
        H=H+2
2620
        DO 1 K=1,K1
        BO 2 L=1,L1
2630
2640
        T(K,L,H)=T(K,L,H-2)
2650
        IF(K.EQ.J1)T(K,L,H)=1000000000.
2660
        IF(L.EQ.J2)T(K,L,M)=1000000000.
2670 2 CONTINUE
2680 1 CONTINUE
2690
       CALL DBACK
2700 5 SUN(N)=SUN(N-2)
2710
        RETURN
2720
        END
2730
         SUBROUTINE DBACK
2740
        CONNON TEMP2(20), TEMP(20), T(18, 18, 30), SUN(50), K1, L1, M
2750
        COMMON PEN(18,18,30), J1, J2, L
2760
       COMMON N(50), IS
2770
        CONMON KEND, LEND, HS, IH, INDX, ID1, ID, DFDR
2780
        COMMON NX(40), IP
2790
         IND=IS
         KT=IND-1
2800
2810
         IF(NX(1).GT.0)G0 T0 7
2820
         IF(IS-2)17,17,19
2830 19
         IS=1
2840
         IP=1
2850
         I=1
2840 21 IF(N(IND).EQ.N(IS))GO TO 3
2870
         IF(IS.EQ.KT)GO TO 1
2880
         IS=IS+2
2890
         GO TO 21
      1 CONTINUE
2900
2910
         IS=2
2920 22 IF(N(KT).EQ.N(IS))GO TO 4
2930
         IF(IS.EQ.IND)GO TO 2
2940
         IS=IS+2
2950
         GO TO 22
2960
      2 CONTINUE
2970
         GO TO 17
2980
      3
         NX(1)=N(KT)
2990
         NX(2)=N(IND)
3000
         NX(3)=N(IS+1)
3010
         1=3
3020
         60 TO 7
      4 MX(1)=N(IS-1)
3030
         NX(2)=N(IS)
3040
```

```
3050
         (GKI)H=(E)XH
3060
         1=3
3070
     7
         IS=1
         IF(N(IS).EQ.NX(I))GO TO 12
3080 23
         IF(IS.EQ.KT)GO TO 6
3090
3100
         IS=IS+2
3110
         GO TO 23
3120
      6 CONTINUE
3130
         GO TO 13
3140 12 I=I+1
3150
         NX(I)=N(IS+1)
3160
         IF(NX(I).EQ.NX(1))GO TO 17
3170
         GO TO 7
3180 13 IS=2
3190 24 IF(N(IS).EQ.NX(1))60 TO 14
         IF(IS.EQ.IND)GO TO 8
3200
3210
         IS=IS+2
3220
         GO TO 24
3230
        CONTINUE
3240
         IF(IP.EQ.I)GO TO 17
3250
         GO TO 15
3260 14
         IK=I
3270
         I=I+1
3280 25 NX(I)=NX(I-1)
3290
         I=I-1
         IF(I.EQ.1)GQ TQ 9
3300
3310
         GO TO 25
3320
      9 CONTINUE
3330
         NX(1)=N(IS-1)
3340
         I=IK+1
3350
         GO TO 7
3360 15
         IK=I
3370
         K5=NX(IK)
3380
         I=1-1
3390 16
         K4=NX(I)
3400
         IF(I.EQ.1.AND.KEND.LE.2)GO TO 18
3410
         T(K5,K4,M)=1000000000.
3420
         IF(I.EQ.1)G0 TO 18
3430
         I=I-1
3440
         GO TO 16
3450
      18 KS=I
3460
         I=IK
3470 17
         IS=IND
3480
         IP=I
3490
         K5=N(IS)
3500
         K4=N(IS-1)
3510
         IF(KEND.EG.1)GO TO 20
3520
         T(K5,K4,M)=1000000000.
3530 20
        RETURN
3540
         END
3550
        SUBROUTINE RISUN
```

```
3560
        CONHON TEMP2(20), TEMP(20), T(18, 18, 30), SUN(50), K1, L1, N
3570
        CONHON PEN(18,18,30),J1,J2,L
3580
       COMMON N(50),IS
        CONHON KEND, LEND, NS, IN, INDX, ID1, ID, DFDR
3590
3600
        COHHON NX(40), IP
3610
         PRINT 1
         FORMAT(///,30X,"ROUTE SEQUENCE")
3620 1
3630
         PRINT 2
3640 2
         FORMAT(///)
3650
         PRINT 3,(NX(LP),LP=1,IP)
3660 3
         FORMAT(18(12,2X))
3670
         DO 4 LX=1, IP
         NX(LX)=0
3680
         CONTINUE
3690 4
3700
         RETURN
3710
         END
```

APPENDIX B
91ST SMW TRANSPORT-ERECTOR ROUTE MAP

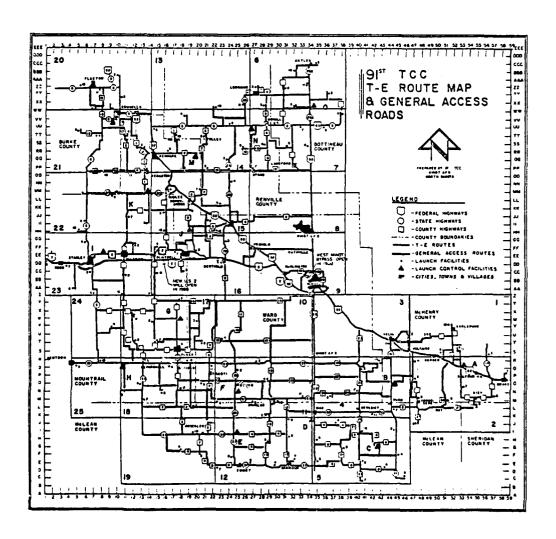


Figure B-1

APPENDIX C
SHORTEST AUTHORIZED ROUTES

TABLE C-1
SHORTEST AUTHORIZED ROUTES FROM THE SMSB

Destination	<u>n</u>		Rou	te of	Trave	<u>1</u>		Mileage
SMSB								00.00
AØ1	83	52						58.00
BØ1	83	52	41					50.50
cø1	83	52	23	6				60.25
DØ1	83							46.50
EØ1	83	23	28					67.25
FØ1	83	23	28					57.25
GØ1	83	14	3					51.50
HØ1	83	14	3	23				73.75
IØ1	83	8	2	to Pai	Lermo	01d	2	55.50
JØ1	83	6	8					32.00
KØ1	83	. 6	52	. 50	1			44.25
LØ1	83	6	52	2	1	17	8	63.75
MØ1	83	6	28	16	7	2		46.50
nø1	83	5						36.50
0 ø 1	83	256						28.00

TABLE C-2
SHORTEST AUTHORIZED ROUTES FROM AØ1

Destination		Route of Travel	Mileage
SMSB	52	83	58.00
AØ1		Road to	00.00
Bø1	52	27 BØ5 41	25.25
CØ1	52	33 2 41 6	40.25
DØ1	52	33 2 41 53 83	46.00
EØ1	52	33 2 41 53 15 4 28 Road by Road by	67.50
FØ1	52	27 BØ5 41 BØ9 22 83 22 2 Cut-off by	28 63.50
GØ1	52	Electric 41 20 23 3 plant	73.25
н ø1	52	Cut-off by Electric 41 20 23 plant	75.75
IØ1	52	2 to Palermo Old 2	91.50
Jø1	52	2 01d 2 8	70.00
KØ1	52	50	86.50
Lø1	52	2 1 17 8	106.25
MØ1	52	7 2	90.00
NØ1	52	28 5	92.00
0ø1	52	83 25 6	86.00

TABLE C-3
SHORTEST AUTHORIZED ROUTES FROM BØ1

Destination			Route of Tra	vel	Mileage
SMSB	41	52 8	3		50.50
AØ1	41	Road	to BØ5 27 5	52	25.25
Bø1					00.00
CØ1	41	6			19.00
DØ1	41	53 8	3		24.50
EØ1	41	24 8	3 53 28		46.75
FØ1	41	24 8 Road			41.25
GØ1	41	Bø1 t	о вø9 23 20	23 3	63.00
нø1	41	Road Bø1 t		0 23	65.50
IØ1	41	52	2 to Palermo	01d 2	84.00
Jø1	41	52	2 01d 2 8		62.50
ĸø1	41	52 5	0		79.00
Lø1	41	52	2 1 17	8	98.75
mø1	41	52	7 2		82.50
nø1	41	52 2	8 5		84.50
0ø1	41	52 8	3 256		78.50

TABLE C-4
SHORTEST AUTHORIZED ROUTES FROM CØ1

Destination			Rou	te of	Trav	<u>rel</u>			Mileage
SMSB	6	23	52	83					60.25
AØ1	6	41	2	33	52				40.25
BØ1	6	41							19.00
cø1									00.00
DØ1	6	21	4	83					18.50
EØ1	6	21	4	83	Max	15	4	28	43.50
FØ1	6	21	4	83	53	28			44.00
GØ1	6	21	4	83	23	3			72.50
HØ1	6	21	4	83	23				75.00
IØ1	6	23	52	2 to	Pale	ermo	01d 2		96.00
. Jø1	6	23	52	2	Old	2	8		74.50
Kø1	6	23	52	50					91.00
LØ1	6	23	52	2	1	17	8		110.75
mø1	6	23	52	7	2				94.50
nø1	6	23	52	28	5				96.50
0 ø 1	6	23	52	83	256				90.50

TABLE C-5
SHORTEST AUTHORIZED ROUTES FROM DØ1

Destination			Rout	e of	Trav	<u>el</u>		Mileage
SMSB	83							46.50
AØ1	83	53	41	2	33	5	52	46.00
BØ1	83	53	41					24.50
cø1	83	4	21	6				18.50
DØ1								00.00
EØ1	83	Max	15	4	28			25.00
FØ1	83	53	28					25.50
GØ1	83	23	3					54.00
нø1	83	23						56.50
IØ1	83	52	2 to	Pal	ermo	C	01d 2	81.50
JØ1	83	52	2	01d	2 8	3		60.00
Kø1	83	52	50	•			·	98.00
Lø1	83	52	2	1	17	8		96.25
mø1	83	52	7	2				80.00
nø1	83	52	28	5				81.75
0 ø 1	83	256						74.50

TABLE C-6
SHORTEST AUTHORIZED ROUTES FROM EØ1

Destination	<u>1</u>	<u>F</u>	Route of Travel	Mileage
SMSB	28	23 83		67.25
AØ1	28	4 15 5	53 41 2 33 52	67.50
BØ1	28	53 83	24 41	46.75
CØ1	28	4 15 N	Max 83 4 21 6	43.50
DØ1	28	4 15 N	Max 83	25.00
EØ1				00.00
FØ1	28			10.00
GØ1	28	23 3		38.25
HØ1	28	23		40.50
IØ1	28	23 3 G)	Ø1 GØ8 2 to Palermo Old 2	69.50
Jø1	28	16 18	9 14 9 2 01d 2 8	60.25
KØ1	28	23 3 G	Ø1 GØ8 2 Old 2 Coulee 50	80.00
LØ1	28	23 3 GØ:	1 GØ8 2 Old 2 50 1 4 2 17 8	103.00
mø1	28	16 18	9. 14 9 28 16 7 2	79.25
nø1	28	16 18	16 11 14 9 28 5	81.25
0 ø 1	28	53 83	256	95.50

TABLE C-7
SHORTEST AUTHORIZED ROUTES FROM FØ1

Destination	<u>1</u>			Rout	e of Travel	Mileage
SMSB	28	23	83		Bood: her Bood has	57.25
AØ1	28	22	83	22	Road by Road by BØ9 41 BØ5 27 52	63.50
Bø1	28	53	83	24	41	41.25
CØ1	28	53	83	4	21 6	44.00
DØ1	28	53	83			25.50
Eø1	28					10.00
FØ1						00.00
GØ1	28	23	3			28.25
нø1	28	23				30.50
IØ1	28	23 3	GØ1	GØ8	2 to Palermo Old 2	59.50
Jø1	28	16	18	9	14 9 2 01d 2 8	50.25
KØ1	28	23	3 G	ø1 0	Ø8 2 01d 2 Coulee 50	70.00
Lø1	28	23	3 GØ	1 GØ	8 2 01d 2 50 1 4 2 17 8	93.00
mø1	28	16	18	9	14 9 28 16 7 2	69.25
nø1	28	16	18	16	11 14 9 28 5	71.25
0 ø1	28	23	83	256		85.25

TABLE C-8
SHORTEST AUTHORIZED ROUTES FROM GØ1

Destination	<u>1</u>		Route of Travel	Mileage
SMSB	3	14	83	51.50
AØ1	3	23	Cut-off by 20 41 electric plant 52	73.25
BØ1	3	23	Road from 20 23 BØ9 to BØ1 41	63.00
CØ1	3	23	By Bø9) 83 4 21 6	72.50
D, 6 1	3	23	83	54.00
Eø1	3	23	28	38.25
FØ1	3	23	28	28.25
GØ1				00.00
нø1	3	23		22.25
IØ1	GØ8	3 2	to Palermo Old 2	31.25
Jø1	GØ8	3 2	01d 2 8	33.00
Kø1	GØ8	8 2	Old 2 to Coulee 50	41.75
Lø1	GØ8	3 2		64.75
mø1	GØ8	8 2	Road by Old 2 to Coulee 52 16 MØ8 2	52.00
nø1	3	14	9 28 5	60.00
0 ø1	3	14	83 256	79.50

TABLE C-9
SHORTEST AUTHORIZED ROUTES FROM HØ1

Destination	<u>1</u>	Route of Travel	Mileage
SMSB	23	3 14 83	73.75
AØ1	23	Cut-off by 20 41 electric plant 52 Road from	75.75
BØ1	23	20 23 BØ9 to BØ1 41 (By BØ9)	65.50
CØ1	23	83 4 21 6	75.00
DØ1	23	83	56.50
EØ1	23	28	40.50
FØ1	23	28	30 .5 0
GØ1	23	3	22.25
нø1		D - 1 1 .	00.00
IØ1	23	Road by G10 Old 2	35.75
Jø1	23	Road by Hø3 and Gø8 2 to Tagus 01d 2 8	46.75
Kø1	23	Road to Palermo 50	46.50
LØ1	23	8 Deal by Deal by Deal by	66.50
mø1	23	Road by Road to Road by Hø3 & Gø8 Coulee 52 16 Mø8 2	68.75
nø1	23	3 14 9 28 5	82.25
0ø1	23	83 256	101.00

TABLE C-10 SHORTEST AUTHORIZED ROUTES FROM IØ1

Destination	Route of Travel	Mileage
SMSB	Old 2 to Palermo 2 8 83	55.50
AØ1	Old 2 to Palermo 2 52	91.50
BØ1	Old 2 to Palermo 2 52 41	84.00
CØ1	Old 2 to Palermo 2 52 23 6	96.00
DØ1	Old 2 to Palermo 2 52 83	81.50
EØ1	Old 2 to Palermo 2 GØ8 GØ1 3 23 28 Old 2	69.50
FØ1	to Palermo 2 GØ8 GØ1 3 23 28	59.50
GØ1	Old 2 to Palermo 2 GØ8	31.25
нø1	Road by Old 2 G1Ø 23	35.75
IØ1		00.00
Jø1	Old 2 8 .	23.00
Kø1	01d 2 Road by KØ7 50	22.75
Lø1	Old 2 8	40.25
mø1	Road to Road by Old 2 Coulee 52 16 MØ8 2	41.75
nø1	Road to Old 2 Coulee 52 16 28 5	61.00
0ø1	Road to Old 2 Coulee 52 16 28 5 256	79.00

TABLE C-11
SHORTEST AUTHORIZED ROUTES FROM JØ1

Destinatio	<u>n</u>		Ī	Route	of Travel	Mileage
SMSB	8	6	83			32.00
AØ1	8	01d 2	2 2	52		70.00
Bø1	8	01d 2	2 2	52	41	62.50
cø1	8	01d 2	2 2	52	23 6	74.50
D, 61	8	01d 2	2	52	83	60.00
EØ1	8	01d 2	9	14	9 18 16 28	60.25
FØ1	8	01d 2	2 9	14	9 18 16 28	50.25
GØ1	8	01d 2	2 2	Gø8		33.00
HØ1	8	01d 2	2 to	Tagu	Road by us 2 GØ8 & HØ3 23	46.75
IØ1	8	01d 2	2			23.00
JØ1					•	00.00
Kø1	8	6	5 5	50		21.00
Lø1	8	6	5 5	52 2	1 17 8	40.00
MØ1	8	6	5	7	2	23.50
nø1	8	6	28	5		36.50
0ø1	8	6	28	5	256	54.50

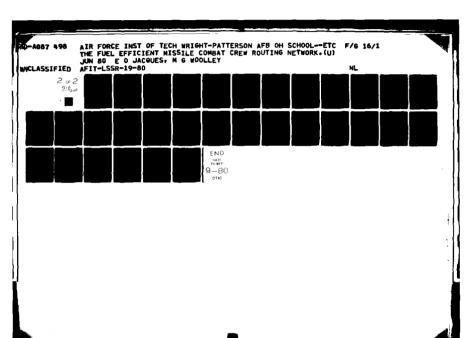


TABLE C-11
SHORTEST AUTHORIZED ROUTES FROM JØ1

Destination	<u>n</u>		į	Route	of	Tra	vel			Mileage
SMSB	8	6	83							32.00
AØ1	8	Old	2 2	52						70.00
B ø1	8	01a	2 2	52	41					62.50
cø1	8	01d	2 2	52	23	6				74.50
D ø1	8	Old	2 2	52	83					60.00
EØ1	8	Old	2 9	14	9	18	16	28		60.25
FØ1	8	Old	2 9	14	9	18	16	28		50.25
GØ1	8	Old	2 2	GØ8	3		. و ـ ـ	.		33.00
HØ1	8	01d	2 to	Tagu	เร	2 G	oad Ø8 &	HØ3	23	46.75
IØ1	8	Old	2	•						23.00
JØ1							•			00.00
Kø1	8	6	5	50						21.00
LØ1	8	6	5	52 2	2	1 1'	7 8			40.00
MØ1	8	6	5	7	2					23.50
nø1	8	6	28	5						36.50
0ø1	8	6	28	5	256					54.50

TABLE C-12
SHORTEST AUTHORIZED ROUTES FROM KØ1

Destination	_]	Rout	<u> </u>	e T	rave	<u>1</u>				Mileage
SMSB	1	50	52	6	83							44.25
AØ1	50	52										86.50
B, ó 1	50	52	41									79.00
Cø1	50	52	23	6								91.00
Dø1	50	52	83									98.00
Eø1	50	Cou]	Lee	01d	2	2	Gø8	GØ1	3	23	28	80.00
FØ1	50	Cow	Lee	Old	2	2	Gø8	GØ1	3	23	28	70.00
GØ1	50	Cou]	Lee	01d	2	2	Gø8					41.75
нø1	50	Roa	ad to	Pa:	Leri	no	23					46.50
I ø1	50	Ros	ad by	KØ:	7	0	ld 2					22.75
Jø1	50	5	6	8								21.00
Kø1 .												00.00
Lø1	1	4	2	17	8							23.25
mø1	1	2										19.00
nø1	1	2	3	5								38.00
0ø1	1	52	5	2	56							56.00

TABLE C-13
SHORTEST AUTHORIZED ROUTES FROM LØ1

Destination	<u>a</u>			F	lout	e o	e I	r	vel					Mileage		
SMSB	8	17	1	2	52	6	8	33						63.75		
AØ1	8	17	1	2	52	:								106.25		
Bø1	8	17	1	2	52	52 41		52 41		98.75						
CØ1	8	17	1	2	52	52 23 6		52 23 6			110.75					
DØ1	8	17	1	2	52	52 83		83		83		83		96.		96.25
eø1	8	17 2	2 4	1	50	01d	2	2	Gø8	GØ1	3	23	28	103.00		
FØ1	8	17	2 4	1	50	Old	2	2	Gø8	GØ1	3	23	28	93.00		
GØ1	8	17	2 4	1	50	Old	2	2	Gø8					64.75		
HØ1	8	23												66.50		
IØ1	8	010	1 2											40.25		
Jø1	8	17	1	2	52	2 5	6	5	8					40.00		
Kø1	8	17	2	4	1	•								23.25		
LØ1														00.00		
mø1	8	17	1	2										25.00		
nø1	8	5	52		5									34.50		
0ø1	8	5	52	9	5 2	256				52.50						

TABLE C-14
SHORTEST AUTHORIZED ROUTES FROM MØ1

Destination	<u>n</u>			Ro	ute	of	Tra	ve1	i			Mileage
SMSB	2	7	16	28	6	83						46.50
AØ1	2	7	52									90.00
BØ1	2	7	52	41							*	82.50
CØ1	2	7	52	23	6	•						96.50
DØ1	2	7	52	83								80.00
EØ1	2	7	16	28	9	14	9 18	16	28			79.25
FØ1	2	7	16 i	28	9 1	4	9 18	16	28			69.25
GØ1	2	M	i by i by		5 52	. C	oule d to		01d 2 Road		cø 8	52.00
HØ1	2	M	g8 1 by	16	52	Co	ulee	2 .d t	Gø8 &	Hø3	23	68.75
IØ1	2		8	1	16	52	Cou					41.75
JØ1	2	7	5	6	8		•					23.50
Kø1	2	1										19.00
LØ1	2	1	17	8	•							25.00
mø1												00.00
nø1	2	3	5									19.00
0ø1	2	3	5	:	256							37.00

TABLE C-15
SHORTEST AUTHORIZED ROUTES FROM NØ1

Destination	<u>1</u>		Route of Travel	Mileage
SMSB	5	83		36.50
AØ1	5	28	52	92.00
BØ1	5	28	52 41	84.50
CØ1	5	28	52 23 6	96.50
DØ1	5	28	52 83	81.75
EØ1	5	28	9 14 11 16 18 16 28	81.25
Fø1	5	28	9 14 11 16 18 16 28	71.25
GØ1	5	28	9 14 3	60.00
HØ1	5	28	9 14 3 23	82.25
IØ1	5	28	Road to 16 52 Coulee Old 2	61.00
JØ1	5	28	6 8	36.50
KØ1	5	3	2 1	38.00
LØ1	5	52	5 8	34.50
mø1	5	3	2	19.00
nø1				00.00
0ø1	5	25	36	18.00

TABLE C-16
SHORTEST AUTHORIZED ROUTES FROM 0Ø1

Destination			Rou	te c	of J	ravel			Mileage
SMSB	256	83							28.00
A,Ø1	256	83	52						86.00
BØ1	256	83	52	41					78.50
CØ1	256	83	52	23	6				90.50
DØ1	256	83							74.50
EØ1	256	83	53	28					95.50
FØ1	256	83	23	28					85.25
G ,6 1	256	83	14	3					79.50
нø1	256	83	23			Road to			101.00
ıø1	256	5	28	16	52	Coulee	Old	2	79.00
JØ1	256	5 2	8 6	8				•	54.50
KØ1	. 256	5	52	1					56.00
lø1	256	5 5	2 5	{	В				52.50
mø1	256	5	3	2					37.00
nø1	256	5							18.00
0,01									00.00

APPENDIX D SHORTEST AUTHORIZED ROUTE DISTANCES

TABLE D-1

0	36.50 28.00	92.00 86.00	84.50 78.50	96.50 90.50	31.75 74.50	31.25 95.50	71.25 85.25	60.00 79.50	82.25 101.00	51.00 79.00	36.50 54.50	38.00 56.00	34.50 52.50	19.00 37.00	00.00 18.00	18.00 00.00
I. M	63.75 46.50 36.50	5.25 90.00 5	3.75 82.50 €	3.75 94.50 9	5.25 80.00 8	3.00 79.25	3.00 69.25 7	4.75 52.00 6	66.50 68.75 82.25	40.25 41.75 61.00	40.00 23.50 36.50	23.25 19.00 38.00	00.00 25.00 34.50	25.00 00.00 19.00	34.50 19.00 00.00	52.50 37.00 18.00
×		00 86.50 100	50 79.00 98	50 91.00 110	00 98 00	25 80.00 10	25 70.00 9	00 41.75 6								
, I	73.75 55.50 32.00 44.25	75.75 91.50 70.00 86.50 106.25 90.00 92.00	65.50 84.00 62.50 79.00 98.75 82.50	75.00 96.00 74.50 91.00 110.75 94.50 96.50	56.50 81.50 60.00 98.00 96.25 80.00 81.75	46.50 69.50 60.25 80.00 103.00 79.25 81.25	30.50 59.50 50.25 70.00 93.00 69.25 71.25	22.25 31.25 33.00 41.75 64.75 52.00 60.00	00.00 35.75 46.75 46.50	35.75 00.00 23.00 22.75	46.75 23.00 00.00 21.00	46.50 22.75 21.00 00.00	66.50 40.25 40.00 23.25	68.75 41.75 23.50 19.00	25 61.00 36.	00 79.00 54.
H U														5 52.00 68.	81.25 71.25 60.00 82.25 61.00 36.50 38.00	95.50 85.25 79.50 101.00 79.00 54.50 56.00
ਜ ਜ	67.25 57.25 51.50	67.50 63.50 73.25	46.75 41.25 63.00	43.50 44.00 72.50	25.00 25.50 54.00	00.00 10.00 38.25	10.00 00.00 28.25	38.25 28.25 00.00	40.50 30.50 22.25	69.50 59.50 31.25	60.25 50.25 33.00	80.00 70.00 41.75	63.75 106.25 98.75 110.75 96.25 103.00 93.00 64.75	46.50 90.00 82.50 94.50 80.00 79.25 69.25 52.00		95.50 85.2
C	60.25 46.50	40.25 46.00	19.00 24.50	00.00 18.50	18.50 00.00	43.50 25.00	44.00 25.50	72.50 54.00	75.00 56.50	96.00 81.50	24.50 60.00	1.00 98.00	0.75 96.25	4.50 80.00	92.00 84.50 96.50 81.75	90.50 74.50
Д	58.00 50.50 6	00.00 25.25 4	25.25 00.00 1	40.25 19.00 0	46.00 24.50 1	67.50 46.75 4	63.50 41.25 4	73.25 63.00 7	75.75 65.50 7	91.50 84.00 9	70.00 62.50 7	44.25 86.50 79.00 91	25 98.75 11	00 82.50 5	00 84.50 \$	86.00 78.50 9
SMSB A	00.00	58.00 00.85	50.50 25.3	60.25 40.	46.50 46.	67.25 67.	57.25 63.	51.50 73.	73.75 75.	55.50 91.	32.00 70.0	44.25 86.	63.75 106.	46.50 90.	36.50 92.0	28.00 86.
	SMSB	ď	Д	ပ	a	េ	ь 88	ဗ	×	н	מ	×	п	Œ	Z	0

APPENDIX E

VEHICLE/DEPLOYMENT STRATEGY COMBINATIONS

TABLE E-1
CARRYALL - DEPLOYMENT STRATEGY I

Day 1 of 3-day Changeover Cycle - 740th SMS

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB - A - SMSB SMSB - B - SMSB SMSB - C - SMSB SMSB - D - SMSB SMSB-F-E-F-SMSB SMSB-G-H-I-H-G-SMSB SMSB-J-L-K-L-J-SMSB SMSB-O-N-M-N-O-SMSB	116.00 101.00 120.50 93.00 134.50 219.00 190.50 130.00	4 4 4 6 6 6 6
Day 2 of 3-day Chang	geover Cyc	cle - 741st SMS
SMSB-B-A-B-SMSB SMSB-D-C-D-SMSB SMSB-F-E-F-SMSB SMSB - G - SMSB SMSB - H - SMSB SMSB - I - SMSB SMSB-J-K-J-SMSB SMSB-J-K-J-SMSB SMSB-M-L-M-SMSB SMSB-O-N-O-SMSB	151.50 130.00 134.50 103.00 147.50 111.00 106.00 143.00 92.00 1118.50	4 4 6 4 4 6 4 4
Day 3 of 3-day Chang	geover Cy	cle - 742nd SMS
SMSB-A-B-C-B-A-SMSB SMSB-D-E-F-E-D-SMSB SMSB-G-H-I-H-G-SMSB SMSB-J-K-J-SMSB SMSB - L - SMSB SMSB - M - SMSB SMSB - N - SMSB SMSB - N - SMSB	204.50 163.00 219.00 106.00 127.50 93.00 73.00 56.00 1042.00	6 6 6 4 4 4 4 4
TOTALS	3265.00	120

TABLE E-2

CARRYALL - DEPLOYMENT STRATEGY II

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB - A - SMSB SMSB - B - SMSB SMSB - C - SMSB SMSB - D - SMSB SMSB -F-E- SMSB SMSB-G-H-I-SMSB SMSB-J-L-K-SMSB SMSB-J-L-K-SMSB	116.00 101.00 120.50 93.00 134.50 165.00 139.50 111.50	4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
Day 2 of 3-day Char	ngeover Cycle	- 741st SMS
SMSB-A-B-C-SMSB SMSB - D - SMSB SMSB -F-E- SMSB SMSB - G - SMSB SMSB - H - SMSB SMSB - I - SMSB SMSB -J-K- SMSB SMSB -J-K- SMSB SMSB -M-L- SMSB SMSB -O-N- SMSB	162.50 93.00 134.50 103.50 147.50 111.00 97.25 135.25 82.50	6 2 6 4 4 4 6 4 4 4 140
Day 3 of 3-day Char	ngeover Cycle	- 742nd SMS
SMSB-A-B-C-SMSB SMSB-D-E-F-SMSB SMSB-G-H-I-SMSB SMSB-J-K-SMSB SMSB-L-SMSB SMSB-L-SMSB SMSB-M-SMSB SMSB-N-SMSB SMSB-N-SMSB	162.50 138.75 165.00 97.25 127.50 93.00 73.00 56.00	6 6 6 4 4 4 4 4
TOTALS	2961.00	120

TABLE E-3

CARRYALL - DEPLOYMENT STRATEGY III

Day 1 of 3-day Changeover Cycle - 740th SMS

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB - A - SMSB SMSB - B - SMSB SMSB - C - SMSB SMSB - D - SMSB SMSB -F-E- SMSB SMSB-G-H-I-SMSB SMSB-J-K-L-SMSB SMSB-J-K-L-SMSB SMSB-O-N-M-SMSB	232.00 202.00 241.00 186.00 269.00 330.00 279.00 223.00	4 4 4 4 6 6 6 6 6 6 40
Day 2 of 3-day Char	ngeover Cycle	- 741st SMS
SMSB-A-B-C-SMSB SMSB - D - SMSB SMSB -F-E- SMSB SMSB - G - SMSB SMSB - H - SMSB SMSB - I - SMSB SMSB -J-K- SMSB SMSB -M-L- SMSB SMSB -M-L- SMSB	325.00 186.00 269.00 207.00 295.00 222.00 194.50 270.50 165.00 2134.00	6 2 6 4 4 4 6 4 4 40
Day 3 of 3-day Cha	ngeover Cycle	- 742nd SMS
SMSB-A-B-C-SMSB SMSB-D-E-F-SMSB SMSB-G-H-I-SMSB SMSB -J-K- SMSB SMSB - L - SMSB SMSB - M - SMSB SMSB - N - SMSB SMSB - N - SMSB	325.00 277.50 330.00 194.50 255.00 186.00 146.00 112.00 1826.00	6 6 6 4 4 4 4 4
TOTALS	5922.00	120

TABLE E-4
STATION WAGON - DEPLOYMENT STRATEGY I

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB - A - SMSB SMSB - B - SMSB SMSB - C - SMSB SMSB - D - SMSB SMSB - E - SMSB SMSB-G-F-G-SMSB SMSB-I-H-I-SMSB SMSB-J-K-J-SMSB SMSB-M-L-M-SMSB SMSB-M-L-M-SMSB SMSB-O-N-O-SMSB	116.00 101.00 120.50 93.00 134.50 159.50 182.50 106.00 143.00 92.00 1248.00	# # # # # # # # # # # # # # # # # # #
Day 2 of 3-day Cha	engeover Cycle	- 741st SMS
SMSB-B-A-B-SMSB SMSB-D-C-D-SMSB SMSB - E - SMSB SMSB - F - SMSB SMSB - G - SMSB SMSB - H - SMSB SMSB - I - SMSB SMSB - J - SMSB SMSB - J - SMSB SMSB-K-L-K-SMSB SMSB-K-L-K-SMSB SMSB-N-D-SMSB	151.50 130.00 134.50 114.50 103.00 147.50 111.00 64.00 135.00 93.00 92.00	4 4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
Day 3 of 3-day Cha	ngeover Cycle	- 742nd SMS
SMSB-3-A-B-SMSB SMSB-D-C-D-SMSB SMSB-F-E-F-SMSB SMSB-G-H-G-SMSB SMSB-J-I-J-SMSB SMSB-J-I-J-SMSB SMSB- K - SMSB SMSB - K - SMSB SMSB - L - SMSB SMSB - L - SMSB SMSB - N - SMSB SMSB - N - SMSB	151.50 130.00 134.50 147.50 110.00 88.50 127.50 93.00 73.00 56.00	4 4 4 4 4 4 4 4 4 4 0
TOTALS	3 635. 50	120

TABLE E-5
STATION WAGON - DEPLOYMENT STRATEGY II

Day 1 of 3-day Changeover Cycle - 740th SMS

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB - A - SMSB SMSB - B - SMSB SMSB - C - SMSB SMSB - D - SMSB SMSB - E - SMSB SMSB - G-F- SMSB SMSB -I-H- SMSB SMSB -J-K- SMSB SMSB -M-L- SMSB SMSB -O-N- SMSB	116.00 101.00 120.50 93.00 134.50 137.00 165.00 97.25 135.25 82.50 1182.00	4 4 4 4 4 4 4 4 4
Day 2 of 3-day Chans	<u>geover Cycle - 7</u>	41st SMS
SMSB -B-A- SMSB SMSB -D-C- SMSB SMSB - E - SMSB SMSB - F - SMSB SMSB - G - SMSB SMSB - H - SMSB SMSB - I - SMSB SMSB - J - SMSB SMSB - J - SMSB SMSB -K-L- SMSB SMSB - M - SMSB SMSB - M - SMSB SMSB - O-N- SMSB	133.75 125.25 134.50 114.50 103.00 147.50 111.00 64.00 131.25 93.00 82.50	44244444444
Day 3 of 3-day Chang	geover Cycle - 7	42nd SMS
SMSB -B-A- SMSB SMSB -D-C- SMSB SMSB -F-E- SMSB SMSB -G-H- SMSB SMSB -J-I- SMSB SMSB -K- SMSB SMSB -L- SMSB SMSB -M- SMSB SMSB -N- SMSB SMSB -O- SMSB	133.75 125.25 134.50 147.50 110.50 88.50 127.50 93.00 73.00 56.00	4 4 4 4 4 4 4 4 4
TOTALS	3511.75	120

TABLE E-6
STATION WAGON - DEPLOYMENT STRATEGY III

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB - A - SMSB SMSB - B - SMSB SMSB - C - SMSB SMSB - D - SMSB SMSB - E - SMSB SMSB -G-F- SMSB SMSB -I-H- SMSB SMSB -J-K- SMSB SMSB -M-L- SMSB SMSB -M-L- SMSB	232.00 202.00 241.00 186.00 269.00 274.00 330.00 194.50 270.50 165.00 2364.00	4 4 4 4 4 4 4 4 4
Day 2 of 3-day Char	ngeover Cycle	- 741st SMS
SMSB -B-A- SMSB SMSB -D-C- SMSB SMSB -E- SMSB SMSB -F- SMSB SMSB -G- SMSB SMSB -H- SMSB SMSB -I- SMSB SMSB -J- SMSB SMSB -K-L- SMSB SMSB -M- SMSB SMSB -O-N- SMSB	267.50 250.50 269.00 229.00 206.00 295.00 222.00 128.00 262.50 186.00 165.00 2480.50	4 2 4 4 4 4 4 2 4 40
Day 3 of 3-day Char	ngeover Cycle	- 742nd SMS
SMSB -B-A- SMSB SMSB -D-C- SMSB SMSB -F-E- SMSB SMSB -G-H- SMSB SMSB -J-I- SMSB SMSB - K - SMSB SMSB - L - SMSB SMSB - M - SMSB SMSB - M - SMSB SMSB - N - SMSB SMSB - O - SMSB	267.50 250.25 269.00 295.00 221.00 177.00 255.00 186.00 146.00 112.00 2178.75	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
TOTALS	7023 .25	120

TABLE E-7

VAN - DEPLOYMENT STRATEGY I

The second secon

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB - A-B-C-B-A - SMSB SMSB - D-E-F-E-D - SMSB SMSE - J-I-H-G-H-I-J - SMSB SMSB-O-N-M-L-K-L-M-N-O-SMSB	163.00 226.00	12 10 8 10 40
Day 2 of 3-day Changeover Cy	ycle - 74	1st SMS
SMSB-A-B-C-D-E-D-C-B-A-SMSB SMSB - G-H-F-H-G - SMSB SMSB - J-I-K-I-J - SMSB SMSB - O-N-L-M-L-N-O - SMSB	208.50 155.50	12 10
Day 3 of 3-day Changeover Cy	ycle - 74	2nd SMS
SMSB - D-C-B-A-B-C-D - SMSB SMSB - G-H-F-E-F-H-G - SMSB SMSB - J-I-L-K-L-I-J - SMSB SMSB - O-N-M-N-O - SMSB	228.50 237.00	8 8 12 <u>12</u> 40
TOTALS	2500.50	120

TABLE E-8

VAN - DEPLOYMENT STRATEGY II

ROUTE	MILES	# OF PEOPLE TRANSPORTED	
SMSB-A-B-C-SMSB SMSB-D-E-F-SMSB SMSB - J-I-H-G-SMSB SMSB-O-N-M-L-K-SMSB	162.50 138.75 164.50 157.50 623.25	12 10 8 10 40	
Day 2 of 3-day Change	over Cycle	- 741st SMS	
SMSB-A-B-C-D-E-SMSB SMSB-G-H-F-SMSB SMSB-J-I-K-SMSB SMSB - O-N-L-M-SMSB	213.00 161.50 122.00 152.00 648.50	10 12 10 8 40	
Day 3 of 3-day Changeover Cycle - 742nd SMS			
SMSB-D-C-B-A-SMSB SMSB-G-H-F-E-SMSB SMSB-J-I-L-K-SMSB SMSB - O-N-M-SMSB	167.25 181.50 162.75 111.50 623.00	8 8 12 <u>12</u> 40	
TOTALS	1894.75	120	

TABLE E-9

VAN - DEPLOYMENT STRATEGY III

ROUTE	MILLES	# OF PEOPLE TRANSPORTED	
SMSB-A-B-C-SMSB SMSB-D-E-F-SMSB SMSB - J-I-H-G-SMSB SMSB-O-N-M-L-K-SMSB	325.00 277.50 329.00 315.00 1246.50	12 10 8 10 40	
Day 2 of 3-day Change	over Cycle -	741st SMS	
SMSB-A-B-C-D-E-SMSB SMSB-G-H-F-SMSB SMSB-J-I-K-SMSB SMSB - O-N-L-M-SMSB	426.00 323.00 244.00 304.00 1297.00	10 12 10 8 40	
Day 3 of 3-day Changeover Cycle - 742nd SMS			
SMSB-D-C-B-A-SMSB SMSB-G-H-F-E-SMSB SMSB-J-I-L-K-SMSB SMSB-O-N-M-SMSB	334.50 363.00 325.50 223.00 1246.00	8 12 12 40	
TOTALS	3789.50	120	

TABLE E-10

29 PAX BUS - DEPLOYMENT STRATEGY I

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB-A-B-C-D-E-D-C-B-A-SMSB	291.50	20
SMSB-O-N-M-L-K-I-H-F-G- J-G-F-H-I-K-L-M-N-O-SMSB	527.00	_20_
0-0-1-11-1-W-H-W-W-G-0W0D	818.50	40
Day 2 of 3-day Changeover C	ycle - 74	1st SMS
SMSB-G-H-F-E-D-C-B- A-B-C-D-E-F-H-G-SMSB	404.00	22
SMSB-0-N-M-L-K-I- J-I-K-L-M-N-0-SMSB	318.00	18
	722.00	40
Day 3 of 3-day Changeover C	ycle - 74	2nd SMS
SMSB-J-I-H-G-E-F-D-C-B- A-B-C-D-F-E-G-H-I-J-SMSB	499.00	20
SMSB-O-N-M-L-K-L-M-N-O-SMSB	226.50 725.50	<u>20</u> 40
Totals	2266.00	120

TABLE E-11
29 PAX BUS - DEPLOYMENT STRATEGY II

ROUTE	MILES	# OF PEOPLE TRANSPORTE	<u>:D</u>
SMSB-A-B-C-D-E-SMSB	213.00	20	
SMSB-O-N-M-L-K- I-H-F-G-J-SMSB	295.50	20	
2 2	508.50	40	
Day 2 of 3-day Changeover SMSB-G-H-F-E-D-C-B-A-SMSE SMSB-O-N-M-L-K-I-J-SMSB		1st SMS 22 18 40	
Day 3 of 3-day Changeover	Cycle - 74	• 2nd SMS	
SMSB-J-I-H-G-E-	307.50	20	
F-D-C-B-A-SMSB SMSB-O-N-M-L-K-SMSB	157.50 465.00	<u>20</u> 40	÷
TOTALS	1424.50	120	

TABLE E-12
29 PAX BUS - DEPLOYMENT STRATEGY III

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB-A-B-C-D-E-SMSB	426.00	20
SMSB-O-N-M-L-K- I-H-F-G-J-SMSB	591.00	20
	1017.00	40
Day 2 of 3-day Changeover	Cycle - 74	1st SMS
SMSB-G-H-F-E-D-C-B-A-SMSB		22
SMSB-0-N-M-L-K-I-J-SMSB	<u>382.00</u> 902.00	<u>18</u> 40
•	,	
Day 3 of 3-day Changeover	Cycle - 74	2nd SMS
SMSB-J-I-H-G-E-		
F-D-C-B-A-SMSB	615.00	20
SMSB-O-N-M-L-K-SMSB	<u>315.00</u> 930.00	<u>20</u> 40
	7,70.00	40
Totals	2849.00	120

TABLE E-13
45 PAX BUS - DEPLOYMENT STRATEGY I

ROUTE	MILES	# OF PEOPLE TRANSPORTED
SMSB-G-H-F-E-D-C-B- A-B-C-D-E-F-H-G-SMSB	404.00	26
SMSB-O-N-M-L-K-I- J-I-K-L-M-N-O-SMSB	318.00	14
	722.00	40
Day 2 of 3-day Changeover	Cycle - 74	1st SMS
SMSB-G-H-F-E-D-C-B- A-B-C-D-E-F-H-G-SMSB	404.00	22
SMSB-O-N-M-L-K-I- J-I-K-L-M-N-O-SMSB	318.00	<u>18</u>
	722.00	40
Day 3 of 3-day Changeover	Cycle - 74	2nd SMS
SMSB-G-H-F-E-D-C-B- A-B-C-D-E-F-H-G-SMSB	404.00	16
SMSB-O-N-M-L-K-I- J-I-K-L-M-N-O-SMSB	318.00	24
	722.00	40
TOTALS	2166.00	120

TABLE E-14
45 PAX BUS - DEPLOYMENT STRATEGY II

ROUTE	MILES	# OF PEOPLE TRANSPORTED		
SMSB-G-H-F-E-D-C-B-A-SMSB SMSB-O-N-M-L-K-I-J-SMSB	260.00 191.00 451.00	26 14 40		
Day 2 of 3-day Changeover Cycle - 741st SMS				
SMSB-G-H-F-E-D-C-B-A-SMSB SMSB-O-N-M-L-K-I-J-SMSB	260.00 191.00 451.00	22 18 40		
Day 3 of 3-day Changeover Cycle - 742nd SMS				
SMSB-G-H-F-E-D-C-B-A-SMSB SMSB-O-N-M-L-K-I-J-SMSB	260.00 191.00 451.00	16 24 40		
TOTALS	1353.00	120		

TABLE E-15
45 PAX BUS - DEPLOYMENT STRATEGY III

ROUTE	MILES	# OF PECPLE TRANSPORTED		
SMSB-G-H-F-E-D-C-B-A-SMSB SMSB-O-N-M-L-K-I-J-SMSB	520.00 382.00 902.00	26 14 40		
Day 2 of 3-day Changeover Cycle - 741st SMS				
SMSB-G-H-F-E-D-C-B-A-SMSB SMSB-O-N-M-L-K-I-J-SMSB	520.00 382.00 902.00	22 <u>18</u> 40		
Day 3 of 3-day Changeover Cycle - 742nd SMS				
SMSB-G-H-F-E-D-C-B-A-SMSB SMSB-O-N-M-L-K-I-J-SMSB	520.00 382.00 902.00	16 24 40		
TOTALS	2706.00	120		

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